DRAINAGE REPORT

For

KIG Silverstrand Walpole, LLC

PROPOSED

"PROPOSED MULTI-FAMILY DEVELOPMENT"

981, 989 & 1015 East Street Walpole, Massachusetts Norfolk County

Prepared by:

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I. EXECUTIVE SUMMARY

This report examines the changes in drainage that can be expected as the result of the development of a proposed multi-family development located on the northerly side of East Street in the Town of Walpole, Massachusetts. The site, which contains approximately 1.9± acres of land on three (3) lots, contains commercial and residential uses consisting of four (4) commercial buildings, two (2) single-family homes, paved and gravel parking areas and driveways, landscaping, and wooded areas.

The proposed project includes the construction of a new 24,650± square-foot six-story multi-family building with 148 total residential units, along with new paved parking areas, driveways, landscaping, storm water management components and associated utilities. This report addresses a comparative analysis of the pre- and post-development site runoff conditions. Additionally, this report provides calculations documenting the design of the proposed stormwater conveyance/management system as illustrated within the accompanying Site Development Plans prepared by Bohler. The project will also provide erosion and sedimentation controls during the demolition and construction periods, as well as long term stabilization of the site.

For the purposes of this analysis the pre- and post-development drainage conditions were analyzed at one (1) "design point" where stormwater runoff currently drains to under existing conditions. This design point is described in further detail in **Section II** below. A summary of the existing and proposed conditions peak runoff rates and volumes for the 2-, 10-, 25-, and 100-year storms can be found in **Table 1.1** and **Table 1.2** below. In addition, the project has been designed to meet or exceed the Massachusetts Department of Environmental Protection (MassDEP) Stormwater Standards and Town of Walpole Stormwater Bylaw to the maximum extent practicable for a redevelopment as further detailed herein.

Table 1.1: Design Point Peak Runoff Rate Summary							

Point of Analysis	2-Year Storm			10-Year Storm			25-Year Storm			100-Year Storm		
	Pre	Post	Δ	Pre	Post	Δ	Pre	Post	Δ	Pre	Post	Δ
DP1	5.17	4.14	-1.03	8.36	7.45	-0.91	10.36	9.72	-0.64	14.58	14.12	-0.46
			*		a set a al lise	whie feet		nd (afa)				

Flows are represented in cubic feet per second (cfs)

Table 1.2. Design I onte volume outinnaly

Point of Analysis	2-Year Storm			10-Year Storm		25-Year Storm			100-Year Storm			
	Pre	Post	Δ	Pre	Post	Δ	Pre	Post	Δ	Pre	Post	Δ
DP1	0.440	0.216	-0.224	0.729	0.455	-0.274	0.912	0.614	-0.298	1.304	0.967	-0.337

*Volumes are represented in acre-feet (ac-ft)

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II. EXISTING SITE CONDITIONS

Existing Site Description

The site, which contains approximately $1.9\pm$ acres of land located on three (3) lots, contains four (4) commercial buildings, two (2) residential homes, paved and gravel parking areas and driveways, landscaping, and some wooded areas.

On-Site Soil Information

Soils within the analyzed area are classified by the Natural Resource Conservation Service (NRCS) as urban land with no Hydrologic Soil Group (HSG) classification.

Onsite soil testing was performed by Bohler in August 2023. Soils consisted of approximately 3.5-7 feet of fill materials underlain by either Sand, Loamy Sand, or Sandy Loam in the locations of the proposed infiltration basins. Estimated seasonal high ground water (ESHGW) was observed at depths ranging from 5.5 to 8.5 feet below grade (fbg). Based upon NRCS mapping and soils discovered during onsite testing, the site is characterized as Hydrologic Soil Group (HSG) 'C', with infiltration rates of 2.41 in/hr at test pits (TP) #2-6 and 1.02 in/hr at TP#1. Refer to **Appendix C** for additional information.

Existing Collection and Conveyance

There are no existing stormwater management or treatment systems installed onsite. Stormwater runoff generated on the commercial parcel to the west is collected via a series of inlets which flow to Spring Brook located north of the Site. Runoff generated on the residential parcels to the east flows overland to the stormwater collection system in East Street and discharges to Spring Brook.

Slopes on the site range from 0.5%-30% with on-site elevations ranging from elevation 146 in the west to elevation 135 at the residential properties in the east.

Existing Watersheds and Design Point Information

For the purposes of this analysis, the pre- and post-development drainage conditions were analyzed at one (1) "design point" as described below where stormwater runoff currently drains to under existing conditions. The minimum time of concentration is calculated as 6 minutes (0.1 hr).

Design Point #1 (DP1) is Spring Brook. Under existing conditions, this design point receives stormwater flows from approximately 1.9± acres of land, designated as sub-catchments "E1", "E2a", and "E2b". Refer to Table 2.2 below for additional detail.

Sub- catchment Name	Total Area (acres)	Cover Description	Curve Number (CN)	Time of Concentration (Tc, minutes)
E1	1.3±	Rooftops, pavement, grass	97	6.0
E2a	0.1±	Pavement, grass	97	6.0
E2b	0.5±	Rooftops, pavement, gravel, grass, woods	82	13.6

Table 2.2: Existing Sub-Catchment Summary

Refer to **Table 1.1 and 1.2** for the existing conditions peak rates of runoff and volumes. Refer to the Existing Conditions Drainage Map in **Appendix D** for a graphical representation of the existing drainage areas.

III. PROPOSED SITE CONDITIONS

Proposed Development, Collection, and Conveyance

The proposed project consists of the construction of a new 24,650± square-foot six-story multifamily building along with associated site, utility, and drainage improvements. The site has been designed so that majority of the paved areas onsite drain to deep-sump, hooded catch basins. Catch basins will capture and convey stormwater runoff, via an underground pipe system, to one of four (4) underground stormwater infiltration systems with isolator rows for additional pretreatment. Runoff from building rooftops will flow to the underground infiltration systems. Overflow from the infiltration systems will discharge to Spring Brook at the northeast corner of the site. A proprietary water quality inlet is proposed to collect and treat runoff from the northeast corner of the site prior to discharge to Spring Brook.

Pipes and associated outlets have been designed for the 100-year storm using the Rational Method.

The best management practices (BMPs) incorporated into the proposed stormwater management system have been designed to meet the standards set forth in the MassDEP Stormwater Handbook. Refer to **Section V** for additional information.

Proposed Watersheds and Design Point Information

The project has been designed to maintain existing drainage watersheds to the greatest extent possible, with the same design points described in **Section II** above. The post-development site was subdivided into seven (7) separate sub catchments for the proposed conditions as described below. The minimum time of concentration is calculated as 6 minutes (0.1 hr).

Under proposed conditions DP#1 receives stormwater flows from approximately 1.9± acres of land, designated as watersheds "P1" through "P6b". Refer to Table 3.1 below for additional detail.

Sub- catchment Name	Total Area (acres)	Cover Description	Curve Number (CN)	Time of Concentration (Tc, minutes)	Hydrologic Routing
P1	0.09±	Pavement, grass	84	6.0	DP#1
P2	0.13±	Pavement, grass	97	6.0	SWM#1 / DP#1
P3	0.47±	Rooftop, pavement, grass	95	6.0	SWM#2 / DP#1
P4	0.45±	Rooftop, pavement, grass	96	6.0	SWM#3 / DP#1
P5	0.20±	Pavement, grass	94	6.0	DP#1
P6a	0.36±	Pavement, grass	94	6.0	SWM#4 / DP#1
P6b	0.20±	Rooftop	98	6.0	SWM#4 / DP#1

Table 3.1: Proposed Sub-catchment Summary

Refer to **Table 1.1 and 1.2** for the calculated proposed conditions peak rates of runoff and volumes. For additional hydrologic information, refer to the Proposed Conditions Drainage Map in **Appendix D** for a graphical representation of the proposed drainage areas.

IV. <u>METHODOLOGY</u>

Peak Flow Calculations

Methodology utilized to design the proposed stormwater management system includes compliance with the guidelines set forth in the latest edition of the Massachusetts DEP Stormwater Handbook. The pre- and post-development runoff rates being discharged from the site were computed using the HydroCAD computer program. The drainage area and outlet information were entered into the program, which routes storm flows based on NRCS TR-20 and TR-55 methods. The other components of the model were determined following standard NRCS procedures for Curve Numbers (CNs) and times of concentrations documented in the appendices of this report. The rainfall data utilized and listed below in **Table 4.1** below for stormwater calculations is based on both Cornell University and NOAA rainfall data. Refer to **Appendix F** for more information.

Frequency	2 year	10 year	25 year	100 year
Rainfall (inches)	3.46*	5.35*	6.53*	9.03**

Table 4.1: Rainfall Intensities

Values derived from NOAA ATLAS 14* and Cornell** on 5/9/23

The proposed stormwater management as designed will provide a decrease in peak rates of runoff and volumes from the proposed facility for the 2-, 10-, 25- and 100-year design storm events. Refer to **Section V** for a description of how the proposed project complies with the MassDEP Stormwater Standards and the Town of Walpole Stormwater Bylaw.

V. STORMWATER MANAGEMENT STANDARDS

The Project falls under M.G.L. Chapter 40B for affordable housing; therefore, local bylaws can be waived as part of the Chapter 40B process if state regulations are met. However, local stormwater regulations were considered and complied with to the maximum extent practicable. The proposed stormwater management system was designed to comply with the MassDEP Stormwater Standards.

Standard #1: No New Untreated Discharges

The project has been designed so that proposed impervious areas shall be collected and passed through the proposed drainage system for treatment prior to discharge.

Standard #2: Peak Rate Attenuation

As outlined in **Tables 1.1 and 1.2**, the development of the site and the proposed stormwater management systems have been designed so that post-development peak rates of runoff and volumes are below pre-development conditions for the 2-, 10-, 25- and 100-year storm events at the design point.

Standard #3: Recharge

The stormwater runoff from the project will be collected and diverted to one of four (4) infiltration systems located onsite. The project as proposed will involve the creation of approximately 4,880 square feet of new impervious area and is required to infiltrate 117 cubic feet of stormwater as defined in Stormwater Standard 3. The proposed infiltration systems are designed to remove sediment from the "first flush" of rainfall and have been sized to retain the first 0.5-inch of runoff from all post-construction impervious surfaces, including the building roof. The four (4) systems

will provide a total of 3,298 cubic feet of volume below the lowest outlet for groundwater recharge. Refer to **Appendix F** of this report for calculations documenting required and provided recharge volumes per Stormwater Standard 3.

The MassDEP Stormwater Standards require that the infiltration BMP drains completely within 72 hours of the end of the storm event. Calculations showing that the proposed infiltration basins will drain within 72 hours are included in **Appendix F** of this report.

Based upon onsite soil testing performed by Bohler in August 2023, separation from the bottom of Stormwater Management areas (SWM) #2-4 to estimated seasonal high groundwater (ESHGW) is greater than four (4) feet; therefore, a groundwater mounding analysis has not been provided. Separation from the bottom of SWM #1 to ESHGW is between 2-4 feet; therefore, exfiltration has been excluded from the hydrologic model and a groundwater mounding analysis has not been has not been provided.

Standard #4: Water Quality

Water quality treatment is provided via deep sump catch basins, a proprietary water quality inlet, isolator rows, and subsurface infiltration systems. The Project proposes to provide a minimum of 44% pretreatment prior to infiltration and a minimum of 80% TSS removal prior to discharge to Spring Brook. TSS removal calculations are included in **Appendix F** of this report.

The project as proposed will involve the creation of approximately $1.7\pm$ total acres of impervious area, including the building rooftop. Per the MassDEP Stormwater Standards, the project is required to treat the 0.5-inch water quality volume, which is equal to 3,036 cubic feet. The proposed infiltration systems provide a total of 3,298 cubic feet of water quality volume below the lowest outlet for water quality treatment. In addition, runoff from impervious areas directed to the water quality inlet in the northeast corner of the site has been sized to treat the 1-inch water quality flow rate. Refer to **Appendix F** of this report for calculations documenting required and provided water quality volumes and flow rates.

Standard #5: Land Use with Higher Potential Pollutant Loads

Not Applicable for this project.

Standard #6: Critical Areas

Not Applicable for this project.

Standard #7: Redevelopment

Although the project is classified as a redevelopment, it has been designed to comply with the MassDEP Stormwater Standards as if it were a new development.

Standard #8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

The proposed project will provide construction period erosion and sedimentation controls as indicated within the site plan set provided for this project. This includes a proposed construction exit, protection for stormwater inlets, protection around temporary material stock piles and various other techniques as outlined on the erosion and sediment control sheets. Additionally, the project is required to file a Notice of Intent with the US EPA and implement a Stormwater Pollution Prevention Plan (SWPPP) during the construction period. The SWPPP will be prepared prior to the start of construction and will be implemented by the site contractor under the guidance and responsibility of the project's proponent.

Standard #9: Operation and Maintenance Plan (O&M Plan)

An Operation and Maintenance (O&M) Plan for this site has been prepared and is included in **Appendix G** of this report. The O&M Plan includes a list of responsible parties and outlines procedures and time tables for the long-term operation and maintenance of the proposed site stormwater management system, including initial inspections upon completion of construction, and periodic monitoring of the system components, in accordance with established practices and the manufacturer's recommendations.

Standard #10: Prohibition of Illicit Discharges

The proposed stormwater system will only convey allowable non-stormwater discharges (firefighting waters, irrigation, air conditioning condensates, etc.) and will not contain any illicit discharges from prohibited sources. An Illicit Discharge Statement is included in **Appendix G**.

VI. <u>SUMMARY</u>

In summary and as outlined in **Table 1.1** and **Table 1.2**, the proposed stormwater management system as designed will provide a decrease in peak rates of runoff and volumes from the proposed facility to Spring Brook for the 2-, 10-, 25- and 100-year storm events. Additionally, the project has been designed to comply with the MassDEP Stormwater Standards as if it were a new development.

APPENDIX A: MASSACHUSETTS STORMWATER MANAGEMENT CHECKLIST



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key.



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Long-term Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



8/30/23 Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development



Mix of New Development and Redevelopment



LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\boxtimes	lo disturbance to any Wetland Resource Areas								
	ite Design Practices (e.g. clustered development, reduced frontage setbacks)								
	Reduced Impervious Area (Redevelopment Only)								
	linimizing disturbance to existing trees and shrubs								
	LID Site Design Credit Requested:								
	Credit 1								
	Credit 2								
	Credit 3								
	lse of "country drainage" versus curb and gutter conveyance and pipe								
	Bioretention Cells (includes Rain Gardens)								
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)								
	reebox Filter								
	Vater Quality Swale								
	Brass Channel								
	Breen Roof								
\boxtimes	Other (describe): Underground Infiltration Systems								

Standard 1: No New Untreated Discharges

- No new untreated discharges
- Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

🖂 Static

Dynamic Field¹

Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

\boxtimes	Recharge B	MPs have be	en sized to	infiltrate the	e Required	Recharge	Volume.
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Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
extent practicable for the following reason:

- Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- \boxtimes Calculations showing that the infiltration BMPs will drain in 72 hours are provided.
- Property includes a M.G.L. c. 21E site or a solid waste landfill and a mounding analysis is included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Standard 3: Recharge (continued)

The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.

Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Checklist ((continued)
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Standard 4: Water Quality (continued)

- The BMP is sized (and calculations provided) based on:
 - The 1/2" or 1" Water Quality Volume or
 - The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
- The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
- A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.

Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)

- The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report.
- The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted **prior to** the discharge of stormwater to the post-construction stormwater BMPs.
- The NPDES Multi-Sector General Permit does *not* cover the land use.
- LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
- All exposure has been eliminated.
- All exposure has *not* been eliminated and all BMPs selected are on MassDEP LUHPPL list.
- The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.

Standard 6: Critical Areas

- The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
- Critical areas and BMPs are identified in the Stormwater Report.



Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

- The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:
 - Limited Project
 - Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
 - Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
 - Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
 - Bike Path and/or Foot Path
 - Redevelopment Project
 - Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.
- The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

APPENDIX B: PROJECT LOCATION MAPS

- USGS MAP
- ➢ <u>FEMA FIRMETTE</u>
- ➢ WALPOLE GIS MAP



USGS MAP

SCALE: 1" = 1,000' SOURCE: MEDFIELD AND NORWOOD MASSACHUSETTS USGS QUADRANGLE

1015 East St Walpole



- Public water supply watersrie
- Retired Public Water Supply
- Scenic/Protected River

🔲 Wildlife Refuge

DEP Wetlands Linear Features

- / SHORELINE
- / HYDROLOGIC CONNECTION
- 🦯 MEAN WATER LINE
- 🖊 APPARENT WETLAND LIMIT
- 🦯 CLOSURE LINE
- EDGE OF INTERPRETED AREA

Potential Vernal Pools

Θ

NHESP Priority Habitats of Rare Species

NHESP Estimated Habitats of Rare Wildlife

NHESP Certified Vernal Pools

*

Areas of Critical Environmental Concern ACECs Boundaries

- 🖊 ROAD/RAIL BASED
- RIVER BASED
- WETLAND BASED
 FLOODPLAIN BASED
- / TIDAL BASED
- CONTOUR BASED
- POLITICAL BOUNDARY
- PROPERTY LINE BASED
- 🖊 OTHER
- / NOT DEFINED

Property Tax Parcels

National Flood Hazard Layer FIRMette



Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

APPENDIX C: SOIL INFORMATION

- > NCRS CUSTOM SOIL RESOURCE REPORT
- SOIL TESTING



USDA Natural Resources

Conservation Service



USDA

Hydrologic Soil Group

	1	1	r	
Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
51	Swansea muck, 0 to 1 percent slopes	B/D	0	0%
602	Urban land, 0 to 15 percent slopes		9.4	78.5%
653	Udorthents, sandy	A	2.6	21.5%
Totals for Area of Intere	st	11.9	100.0%	

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition Component Percent Cutoff: None Specified Tie-break Rule: Higher



Site Location or	lot #	981, 98	9, & 1015 East Main Street, Walpole, MA DEEP HOLE # 1									
Applicant/owne	r:	KIG Silv	erstrand V	Valpole,	, LLC							
DATE:	08/1	7/2023		WEAT	THER:	Cloud	y	TEMF	- : 70	0		
LOCATION: (R	efer to	sketch at	tached)			•						
PERFORMED I	BY:	Connor	Ennis (SE	#14656) Bohler							
WITNESSED B	Y:	N/A (fo	r drainage	only)								
Land Use:	Vaca	nt / Com	mercial			Landfo	orm:	Mora	ine			
Vegetation:	None	2				Slope:		0-3%				
Stone Walls:	ΠY		Surfac	e Stones	s: 🗌 Y	\triangleright	N 🛛					
Distance From:												
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Are	a:		> 10	00 ft.		
Drinking Water Well:			>100 ft.		Drainagev	vay:			>10	00 ft.		
Property Line:			> 10 ft.		Other: N/	4						
DEEP OBSE	RVA		OLE LOO	3								
Depth	Soil Horizon Soil Texture Soil C				Soil Co	olor	Other:	Structures	s; Sto	ones; Bou gravel	ılders;	Consistency; %
0"-84"	FILL						Mix of f brick	of fill, crushed stone, scattered asphalt and				asphalt and
84"-96"	C1		Sandy Loam 10YR 6/3				Massive, friable, redox observed at 84", 5% gravel, strongly stained fingers, formed strong cast					84", 5% gravel, ng cast
96" - 108"	C2		Sandy L	oam	10YR 7/2		Massive, friable, strongly stained fingers, formed strong cast, distinct color change					
108" - 120" +	C3		Sand		10YR 6/3	10YR 6/3Gravelly sand, single grain, loose, 5-10and stones				10% cobbles		
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock:			120" (+)			
Depth to Groun	dwater	:	Standing	Water i	n Hole:	96"						
			Weeping	From P	Pit Face:	96"						
			Estimated	d Seasc	onal High Gro	undwat	er:		84'	11		
DETERMINATI	ON FC	R SEAS	ONAL HIG	H WAT	ER TABLE							
Method used:			Depth obs	erved st	anding in obs.	hole:		96"				
			Depth to w	eeping f	from side of ob	s. hole:		96"				
			Depth to s	oil mottle	es, description:			84"				
			Groundwa	ter adjus	stment:			NA		<u>.</u>		-
Index Well #: NA Reading Date: NA					NA	Index \ Level:	Vell	NA		Adj. Fac	ctor:	NA
Adj. ground wate	r level:											
Notes:	Top la indica	iyer is mi tive of se	x of fill, sca asonal hig	attered h wate	debris of asp r table; weep	halt and ing obs	d brick; re erved at !	edoximorı 96"; stanc	phic f ding v	features water ob:	observ served	ved at 84" at 96"

Site Location or	lot #	981, 98	9, & 1015	, & 1015 East Main Street, Walpole, MA DEEP HOLE # 2								
Applicant/owne	r:	KIG Silv	erstrand V	Valpole, I	LLC							
DATE:	08/1	7/2023		WEATH	HER:	Cloud	y	TEM	P: 70	0		
LOCATION: (R	efer to	sketch at	tached)									
PERFORMED	BY:	Connor	Ennis (SE i	#14656)	Bohler							
WITNESSED B	Y:	N/A (foi	⁻ drainage	only)								
Land Use:	Resid	dential				Landfo	orm:	Mora	aine			
Vegetation:	Gras	S				Slope:		3-5%				
Stone Walls:		Surfac	e Stones	s: 🗌 Y	\triangleright	א ⊵						
Distance From:												
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Are	a:		> 10	00 ft.		
Drinking Water Well:			>100 ft.		Drainagev	vay:			>10)0 ft.		
Property Line:			> 10 ft.		Other: N/A	4						
DEEP OBSE	RVA		DLE LOO	3	•							
Depth	Depth Soil Horizon Soil Texture Soil G					olor	Other:	Structure	s; Sto	nes; Bou gravel	ulders;	Consistency; %
0"-42"	FILL		-		-		Mix of	Mix of fill, crushed stone				
42"-54"	А		Loamy Sand 10YR 2/2 Granular, friable, %5 gravel, 5% cob					% cobb	les & stones			
54" - 84"	C1		Loamy S	Sand	10YR 7/1		Fine loamy sand, Massive, friable, redox & weeping observed at 66", did not stain fingers, more					
84" - 102" +	C2		Sand		10YR 7/2		Gravell and sto	y sand, si ones	ngle g	grain, loo	se, 5-1	.0% cobbles
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock:			102" (+)			
Depth to Groun	dwater	:	Standing	Water in	Hole:	96"						
			Weeping	From Pit	Face:	42" &	66"					
			Estimated	d Season	nal High Gro	undwate	er:		66"			
DETERMINATI	ON FC	R SEAS	ONAL HIG	H WATE	RTABLE							
Method used:			Depth obs	erved sta	nding in obs.	hole:		96"				
			Depth to w	eeping fro	om side of ob	s. hole:		66"				
			Depth to s	oil mottles	s, description:			66"				
			Groundwater adjustment:			lun al a v V	A/all	NA				1
Index Well #: NA Reading Date: NA					4	Level:	ven	NA		Adj. Fac	ctor:	NA
Adj. ground wate	r level:											
	Top la	iyer is mi	k of fill; we	eping fir	rst observed	at 42"	is not inc	dicitive of	seaso	onal high	groun	dwater
Notes:	(Incor	isistent, o ervation	niy obers	eved in s imorphic	ingle location	on, cons	istently (ary soll sa	mples 6" ind	s delow v licative o	weepin	ig in Snal high water
	table;	standing	water obs	served at	t 96"; large l	boulder	observe	d at 60"	5 110		1 35920	anai mgir water

Site Location or	lot #	981, 98	O, & 1015 East Main Street, Walpole, MADEEP HOLE # 3											
Applicant/owne	r:	KIG Silv	erstrand W	/alpole,	LLC									
DATE:	08/1	7/2023		WEAT	HER:	Cloud	y	TEMF	Þ: 70	0				
LOCATION: (R	efer to	sketch at	tached)					·						
PERFORMED I	BY:	Connor	Ennis (SE #	<i>‡</i> 14656)	Bohler									
WITNESSED B	Y:	N/A (fo	r drainage	only)										
Land Use:	Vaca	nt / Com	mercial			Landfo	orm:	Mora	ine					
Vegetation:	None		Slope		0-3%									
Stone Walls:	ΠY	🛛 N				Surfac	e Stones	s: 🗌 Y		⊠ N				
Distance From:														
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Are	a:		> 1	00 ft.				
Drinking Water Well:			>100 ft.		Drainagev	vay:			>10	00 ft.				
Property Line:			> 10 ft.		Other: N/	٩								
DEEP OBSE	RVA	ΓΙΟΝ Η	OLE LOG	3										
Depth	Soil Horizon Soil Texture Soil C					olor	Other:	Structures	s; Sto	ones; Bou gravel	lders;	Consistency; %		
0"-78"	FILL		-		-		Mix of f brick	Aix of fill, construction backfill material & scarrick			l, construction backfill material			
78"-90"	А		Sand 10YR 6/				Buried organic	ed organic layer, sand with high percentage of anics, granular, friable, weeping observed at 78"						
90" - 108" +	C1		Sand 10YR 7/2				Gravell and sto	y sand, sir nes	ngle g	grain, loos	se, 5-1	10% cobbles		
	-		-											
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock:			108" (+)					
Depth to Groun	dwater	:	Standing	Water i	n Hole:	None								
			Weeping	From P	it Face:	78"								
			Estimated	l Seaso	nal High Gro	undwat	er:		78'	11				
DETERMINATI	ON FC		ONAL HIG	H WAT	ER TABLE									
Method used:			Depth obse	erved sta	anding in obs.	hole:		NA						
			Depth to w	eeping f	rom side of ob	s. hole:		78"						
			Depth to se	oil mottle	es, description:			NA						
			Groundwat	ter adjus	tment:			NA						
Index Well #: NA Reading Date: NA					IA	Index \ Level:	Vell	NA		Adj. Fac	tor:	NA		
Adj. ground wate	r level:													
Notes:	Top la indica	iyer is mi tive of se	x of fill, bri asonal hig	ck, cons h water	struction bac table; pit te	kfill ma rminate	terial, col ed at 108'	bbles, and " due to e	l stor xcava	nes; weep ator restr	ing ol	oserved at 78" s.		

Site Location or	lot #	981, 98	9, & 1015 East Main Street, Walpole, MA DEEP HOLE # 4										
Applicant/owne	r:	KIG Silv	erstrand V	/alpole, l	LC								
DATE:	08/1	7/2023		WEATH	IER:	Cloud	y	TEM	P: 70 °				
LOCATION: (R	efer to	sketch at	tached)					·					
PERFORMED I	BY:	Connor	Ennis (SE #	‡14656)	Bohler								
WITNESSED B	Y:	N/A (foi	r drainage	only)									
Land Use:	Vaca	nt / Com	mercial			Landfo	orm:	Mora	ine				
Vegetation:	None	j				Slope:		0-3%					
Stone Walls:	Υ	🛛 N				Surfac	e Stones	s: 🗌 Y	\boxtimes	Ν			
Distance From:													
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Are	a:		> 100	D ft.			
Drinking Water Well:			>100 ft.		Drainagev	vay:			>100) ft.			
Property Line:			> 10 ft.		Other: N/	Ą							
DEEP OBSE	RVA	FION HO	OLE LOC	3									
Depth	Soil	Horizon Soil Texture Soil (olor	Other:	Structures	s; Ston	es; Boulde gravel	ers;	Consistency; %	
0"-84"	FILL						Mix of t brick	f fill, crushed stone, scattered asphalt and					
84"-102"	C1	Sand			10YR 6/3Gravelly sand stones, stand			y sand, sir standing	ngle gra water	ain, loose, observed	5-1 at 8	0% cobbles & 4"	
	-		-										
	-		-										
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock: 1				102" (+)			
Depth to Groun	dwater	:	Standing	Water in	Hole:	84"							
			Weeping	From Pit	Face:	None							
			Estimated	I Season	al High Gro	undwate	er:		84"				
DETERMINATI	ON FC	R SEAS	ONAL HIG	H WATE	R TABLE								
Method used:			Depth obs	erved star	nding in obs.	hole:		84"					
			Depth to w	eeping fro	om side of ob	s. hole:		NA					
			Depth to s	oil mottles	, description:	:		NA					
			Groundwater adjustment:					NA				1	
Index Well #: NA Reading Date: NA						Index V	Vell	NA		Adj. Factor:		NA	
Adj. ground wate	r level:												
Notes:	Top la obser restric	iyer is mi ved at 84 ctions	x of fill, sca " indicativ	attered d e of seas	ebris of asp onal high w	halt and ater tak	d brick; a ble; pit te	sphalt lay rminated	er obso at 102	erved at 24 " due to e	4"; s xcav	standing water vator	

Site Location or	lot #	981, 98	DescriptionDescripti										
Applicant/owne	r:	KIG Silve	erstrand W	/alpole,	LLC					•			
DATE:	08/1	7/2023		WEATH	HER:	Cloud	y	TEM	P: 70	0			
LOCATION: (R	efer to	sketch at	tached)										
PERFORMED I	BY:	Connor	Ennis (SE i	#14656)	Bohler								
WITNESSED B	Y:	N/A (foi	r drainage	only)									
Land Use:	Vaca	nt / Com	mercial			Landfo	orm:	Mora	aine				
Vegetation:	None	9				Slope:		0-3%					
Stone Walls:	Υ	N 🛛				Surfac	e Stones	s: 🗌 Y	\triangleright	⊠ N			
Distance From:													
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Are	a:		> 10	00 ft.			
Drinking Water Well:			>100 ft.		Drainagev	vay:			>10	00 ft.			
Property Line:			> 10 ft.		Other: N//	Ą							
DEEP OBSE	RVA	ΓΙΟΝ Η	OLE LOC	3									
Depth	epth Soil Horizon Soil Texture Soil (olor	Other:	Structures	s; Sto	nes; Boul gravel	ders;	Consistency; %	
0"-84"	FILL		-	- Mix of fill, construction backfill mater					rial				
84"-96"	А		Sand		10YR 2/2		Buried organic layer, sand with high percentage of organics, granular, friable, weeping observed at 84"						
96" - 126" +	C1		Sand		10YR 6/3		Gravell stones	Gravelly sand, single grain, loose, 5-10% cobbles & stones					
	-		-										
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock: 12				126" (+)			
Depth to Groun	dwater	:	Standing	Water in	Hole:	96"							
			Weeping	From Pit	Face:	84"							
			Estimated	Seasor	al High Gro	undwate	er:		84"	I			
DETERMINATI	ON FC	R SEAS	ONAL HIG	H WATE	RTABLE								
Method used:			Depth obs	erved sta	nding in obs.	hole:		96"					
			Depth to w	eeping fr	om side of ob	s. hole:		84"					
			Depth to s	oil mottles	s, description			NA					
Groundwater adjustment:								NA					
Index Well #: NA Reading Date: NA						Level:	vell	NA		Adj. Fact	or:	NA	
Adj. ground wate	r level:												
Notes:	Top la	iyer is mi	x of fill; we	eping of	oserved at 8	4"; stan	iding wat	ter observ	ved at	: 96"			

Site Location or	lot #	981, 98	9, & 1015 East Main Street, Walpole, MA DEEP HOLE # 6									IOLE # 6	
Applicant/owne	r:	KIG Silve	erstrand W	/alpole,	LLC								
DATE:	08/1	7/2023		WEATH	HER:	Cloudy	y	TEM	P: 70	0			
LOCATION: (R	efer to	sketch at	tached)										
PERFORMED I	BY:	Connor	Ennis (SE #	#14656)	Bohler								
WITNESSED B	Y:	N/A (foi	r drainage	only)									
Land Use:	Vaca	nt / Com	mercial			Landfo	orm:	Mora	aine				
Vegetation:	None	j				Slope:		0-3%					
Stone Walls:	Υ	🛛 N				Surfac	e Stones	s: 🗌 Y	\triangleright	N			
Distance From:													
Open Water Bo	dies:		> 100 ft.		Possible V	Vet Area	a:		> 10	00 ft.			
Drinking Water Well:			>100 ft.		Drainagev	vay:			>10	0 ft.			
Property Line:			> 10 ft.		Other: N//	Ą							
DEEP OBSE	RVA	FION HO	OLE LOC	3									
Depth	h Soil Horizon Soil Texture Soil				Soil Co	olor	Other:	Structures	s; Stoi	nes; Boulde gravel	ers;	Consistency; %	
0"-84"	FILL		- Mix of fill, crush brick				fill, crushe	hed stone, scattered asphalt and					
84"-96"	А		Sand		10YR 2/2		Buried organic layer, sand with high percentage of organics, granular, friable					percentage of	
96" - 114"	C1		Sand		10YR 6/3		Gravelly sand, single grain, loose, 5-10% cobbles and stones, weeping observed at 102"						
114" - 120" +	C2		Loamy S	and	10YR 7/1		Massiv fingers	Massive, friable, formed weak cast, slightly stained fingers, 0-5% gravel, 0-5% cobbles					
Parent Material	(geolo	gic):	Glacial O	utwash		Depth to Bedrock:				120" (+)			
Depth to Groun	dwater	:	Standing	Water in	Hole:	102"							
			Weeping	From Pit	t Face:	102"							
			Estimated	Seasor	nal High Gro	undwate	er:		102	"			
DETERMINATI	ON FC	R SEAS	ONAL HIG	H WATE	R TABLE								
Method used:			Depth obs	erved sta	nding in obs.	hole:		102"					
			Depth to w	eeping fr	om side of ob	s. hole:		102"					
			Depth to s	oil mottles	s, description:	:		NA					
			Groundwa	ter adjust	ment:			NA					
Index Well #:	NA		Reading D	ate: N	Α	Index V	vell	NA		Adj. Factor	:	NA	
Adj. ground wate	r level:												
Notes:	Top la seaso	iyer is miz nal high v	x of fill, sca vater table	attered o e; standi	lebris of asp ng water ob	halt and served a	d brick; v at 96"	veeping o	bservo	ed at 102 ir	ndic	ative of	
APPENDIX D: EXISTING CONDITIONS HYDROLOGIC ANALYSIS

- > EXISTING CONDITIONS DRAINAGE MAP
- > EXISTING CONDITIONS HYDROCAD COMPUTATIONS







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 Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
 1	2-YR	Type III 24-hr		Default	24.00	1	3.46	2
2	10-YR	Type III 24-hr		Default	24.00	1	5.35	2
3	25-YR	Type III 24-hr		Default	24.00	1	6.53	2
4	100-YR	Type III 24-hr		Default	24.00	1	9.03	2

Rainfall Events Listing

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Area Listing (selected nodes)

Area	CN	Description	
(acres)		(subcatchment-numbers)	
0.251	74	>75% Grass cover, Good, HSG C (E1, E2a, E2b)	
0.076	89	Gravel roads, HSG C (E2b)	
1.090	98	Paved parking, HSG C (E1, E2a, E2b)	
0.395	98	Roofs, HSG C (E1, E2b)	
0.095	70	Woods, Good, HSG C (E2b)	
1.907	93	TOTAL AREA	

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Soil Listing (selected nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
1.907	HSG C	E1, E2a, E2b
0.000	HSG D	
0.000	Other	
1.907		TOTAL AREA

Existing HydroCAD

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Ground Covers (selected nodes)										
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground	Subcatchment			
 (acres)	(acres)	(acres)	(acres)	(acres)	(acres)	Cover	Numbers			
0.000	0.000	0.251	0.000	0.000	0.251	>75% Grass cover, Good	E1,			
							E2a,			
							E2b			
0.000	0.000	0.076	0.000	0.000	0.076	Gravel roads	E2b			
0.000	0.000	1.090	0.000	0.000	1.090	Paved parking	E1,			
							E2a,			
							E2b			
0.000	0.000	0.395	0.000	0.000	0.395	Roofs	E1, E2b			
0.000	0.000	0.095	0.000	0.000	0.095	Woods, Good	E2b			
0.000	0.000	1.907	0.000	0.000	1.907	TOTAL AREA				

	Existing HydroCAD
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Pipe Listing (selected nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)
1	E1	0.00	0.00	83.0	0.0010	0.013	0.0	8.0	0.0
2	E1	0.00	0.00	99.0	0.0050	0.013	0.0	10.0	0.0
3	E1	0.00	0.00	76.0	0.0013	0.013	0.0	12.0	0.0
4	E1	0.00	0.00	26.0	0.0230	0.013	0.0	12.0	0.0
5	E2a	0.00	0.00	413.0	0.0040	0.013	0.0	36.0	0.0
6	E2b	0.00	0.00	413.0	0.0040	0.013	0.0	36.0	0.0

REV0 - W211263-EX Prepared by Bohler Engineers <u>HydroCAD® 10.20-2g_s/n 03478_© 2022 Hydro</u>	oCAD Software So	Ty	pe III 24-hr	Existing HydroCAD 2-YR Rainfall=3.46 Printed 8/23/2023 Page 7	" }
Time span=0.00 Runoff by SCS TR Reach routing by Dyn-Stor-Inc	-72.00 hrs, dt=0.0 R-20 method, UH= d method - Pond	15 hrs, 1441 SCS, Weig routing by	points hted-CN Dyn-Stor-Ind	l method	
SubcatchmentE1: North / Central - Drain	Runoff Area=1.3 Flow Length=543'	17 ac 96.09 Tc=6.0 min	5% Imperviou CN=97 Ru	s Runoff Depth=3.11" inoff=4.27 cfs 0.342 af	
SubcatchmentE2a: South - Overland	Runoff Area=0.1 Flow Length=836'	03 ac 95.1 Tc=6.0 min	5% Imperviou CN=97 Ru	s Runoff Depth=3.11" inoff=0.33 cfs 0.027 af	
SubcatchmentE2b: Southeast - Overland F	Runoff Area=0.4 Now Length=539	87 ac 25.09 Tc=13.6 min	5% Imperviou CN=82 Ru	s Runoff Depth=1.75" inoff=0.78 cfs 0.071 af	
Link DP1: Spring Brook			lr Prir	nflow=5.17 cfs 0.440 af mary=5.17 cfs 0.440 af	:

Total Runoff Area = 1.907 acRunoff Volume = 0.440 afAverage Runoff Depth = 2.77"22.13% Pervious = 0.422 ac77.87% Impervious = 1.485 ac

Summary for Subcatchment E1: North / Central - Drain Infrastructure

4.27 cfs @ 12.09 hrs, Volume= Runoff = Routed to Link DP1 : Spring Brook

0.342 af, Depth= 3.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area	(ac) C	N Dese	cription						
0.	052 7	'4 >75°	% Grass co	over, Good,	HSG C				
0.	287 9	8 Roo	fs, HSG C						
0.	978 9	8 Pave	ed parking	, HSG C					
1.3	1.317 97 Weighted Average								
0.	052	3.95	% Perviou	s Area					
1.	265	96.0	5% Imperv	/ious Area					
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
0.4	50	0.0586	1.91		Sheet Flow, 145.28-142.35				
					Smooth surfaces n= 0.011 P2= 3.46"				
1.1	209	0.0236	3.12		Shallow Concentrated Flow, 142.35-137.41				
					Paved Kv= 20.3 fps				
1.3	83	0.0010	1.09	0.38	Pipe Channel, 133.7-133.7				
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'				
					n= 0.013 Corrugated PE, smooth interior				
0.6	99	0.0050	2.84	1.55	Pipe Channel, 133.5-133				
					10.0" Round Area= 0.5 sf Perim= 2.6' r= 0.21'				
					n= 0.013 Corrugated PE, smooth interior				
0.8	76	0.0013	1.64	1.28	Pipe Channel, 132.9-132.8				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013 Corrugated PE, smooth interior				
0.1	26	0.0230	6.88	5.40	Pipe Channel, 132.6-132				
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'				
					n= 0.013 Corrugated PE, smooth interior				
4.3	543	Total. I	ncreased t	o minimum	Tc = 6.0 min				

Total, Increased to minimum Tc = 6.0 min 545

Summary for Subcatchment E2a: South - Overland

Runoff 0.33 cfs @ 12.09 hrs, Volume= 0.027 af, Depth= 3.11" = Routed to Link DP1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area (ac)	CN	Description		
0.005	74	>75% Grass cover, Good, HSG C		
0.098	98	Paved parking, HSG C		
0.103	97	Weighted Average		
0.005		4.85% Pervious Area		
0.098		95.15% Impervious Area		

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Existing HydroCAD *Type III 24-hr 2-YR Rainfall=3.46"* Printed 8/23/2023 <u>Solutions LLC Page 9</u>

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.5	50	0.0420	1.68		Sheet Flow, 144.9-142.8
					Smooth surfaces n= 0.011 P2= 3.46"
2.6	373	0.0140	2.40		Shallow Concentrated Flow, 142.8-137.74
					Paved Kv= 20.3 fps
1.2	413	0.0040	5.97	42.18	Pipe Channel, 133.7-132
					36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
					n= 0.013 Corrugated PE, smooth interior
1 2	026	Total I	norogod t	o minimum	$T_{0} = 6.0 \text{ min}$

4.3 836 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment E2b: Southeast - Overland

Runoff	=	0.78 cfs @	12.19 hrs,	Volume=	0.071 af,	Depth= 1.75"
Routed	d to Linl	k DP1 : Spring	Brook			

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 2-YR Rainfall=3.46"

_	Area	(ac) C	N Des	cription		
	0.	108 9	98 Roo	fs, HSG C		
	0.	076 8	39 Grav	vel roads, l	HSG C	
	0.	095	70 Woo	ods, Good,	HSG C	
	0.	194	74 >759	% Grass c	over, Good	, HSG C
_	0.	014 9	98 Pave	ed parking	, HSG C	
	0.	487 8	32 Wei	ghted Aver	age	
	0.	365	74.9	5% Pervio	us Area	
	0.	122	25.0	5% Imperv	vious Area	
	-				A B	
		Length	Slope	Velocity	Capacity	Description
	(min)	(teet)	(π/π)	(ft/sec)	(CIS)	
	9.0	30	0.0150	0.06		Sheet Flow, 140.2-139.75
						Grass: Bermuda n= 0.410 P2= 3.46"
	2.6	20	0.1380	0.13		Sheet Flow, 139.75-137
	~ -			4.04		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.7	50	0.0300	1.21		Shallow Concentrated Flow, 137-135.5
	0.4	00	0 0070	0.04		Short Grass Pasture Kv= 7.0 fps
	0.1	26	0.0270	3.34		Shallow Concentrated Flow, 138.43-137.74
	10	440	0.0040	E 07	10 10	Paved $KV = 20.3$ fps
	1.2	413	0.0040	5.97	42.10	Pipe Channel, 133.7-132 26.0" Bound Aroos 7.1 of Borims 0.4' rs 0.75'
						50.0 Rouliu Alea- 7.1 Si Felilii- 9.4 I- 0.75
_	40.0		Tatal			
	13.6	539	Iotal			

Summary for Link DP1: Spring Brook

Inflow A	rea =	1.907 ac, 77.	87% Impervious,	Inflow Depth = 2	.77" for 2-YR event
Inflow	=	5.17 cfs @ 12	2.09 hrs, Volume	e 0.440 af	
Primary	=	5.17 cfs @ 12	2.09 hrs, Volume	e 0.440 af	, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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Time span=0.00-72.00 hrs, dt=0.05 hr Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond rou	s, 1441 points 5, Weighted-CN ting by Dyn-Stor-Inc	d method
SubcatchmentE1: North / Central - Drain Runoff Area=1.317 a	c 96.05% Imperviou	is Runoff Depth=5.00"
Flow Length=543' Tc=	6.0 min CN=97 Rเ	unoff=6.69 cfs 0.548 af
SubcatchmentE2a: South - Overland Runoff Area=0.103 a	c 95.15% Imperviou	is Runoff Depth=5.00"
Flow Length=836' Tc=	6.0 min CN=97 Rเ	unoff=0.52 cfs 0.043 af
SubcatchmentE2b: Southeast - Overland Runoff Area=0.487 a	c 25.05% Imperviou	is Runoff Depth=3.39"
Flow Length=539' Tc=1	3.6 min CN=82 Rເ	unoff=1.50 cfs 0.138 af
Link DP1: Spring Brook	lı Pri	nflow=8.36 cfs 0.729 af mary=8.36 cfs 0.729 af

Total Runoff Area = 1.907 acRunoff Volume = 0.729 afAverage Runoff Depth = 4.59"22.13% Pervious = 0.422 ac77.87% Impervious = 1.485 ac

Summary for Subcatchment E1: North / Central - Drain Infrastructure

6.69 cfs @ 12.09 hrs, Volume= Runoff = Routed to Link DP1 : Spring Brook

0.548 af, Depth= 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area	(ac) C	N Dese	cription		
0.	052 7	'4 >75°	% Grass c	over, Good,	, HSG C
0.	287 9	8 Roo	fs, HSG C		
0.	978 9	8 Pave	ed parking	, HSG C	
1.	317 9	7 Weid	ahted Aver	ade	
0.	052	3.95	% Perviou	s Area	
1.	265	96.0	5% Imperv	/ious Area	
			•		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.4	50	0.0586	1.91		Sheet Flow, 145.28-142.35
					Smooth surfaces n= 0.011 P2= 3.46"
1.1	209	0.0236	3.12		Shallow Concentrated Flow, 142.35-137.41
					Paved Kv= 20.3 fps
1.3	83	0.0010	1.09	0.38	Pipe Channel, 133.7-133.7
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
					n= 0.013 Corrugated PE, smooth interior
0.6	99	0.0050	2.84	1.55	Pipe Channel, 133.5-133
					10.0" Round Area= 0.5 sf Perim= 2.6' r= 0.21'
					n= 0.013 Corrugated PE, smooth interior
0.8	76	0.0013	1.64	1.28	Pipe Channel, 132.9-132.8
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.1	26	0.0230	6.88	5.40	Pipe Channel, 132.6-132
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
4.3	543	Total. I	ncreased t	o minimum	Tc = 6.0 min

Total, Increased to minimum Tc = 6.0 min 545

Summary for Subcatchment E2a: South - Overland

Runoff 0.52 cfs @ 12.09 hrs, Volume= 0.043 af, Depth= 5.00" = Routed to Link DP1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area (ac)	CN	Description
0.005	74	>75% Grass cover, Good, HSG C
0.098	98	Paved parking, HSG C
0.103	97	Weighted Average
0.005		4.85% Pervious Area
0.098		95.15% Impervious Area

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Existing HydroCAD Type III 24-hr 10-YR Rainfall=5.35" Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC Printed 8/23/2023 Page 13

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	50	0.0420	1.68	X /	Sheet Flow, 144.9-142.8
					Smooth surfaces n= 0.011 P2= 3.46"
2.6	373	0.0140	2.40		Shallow Concentrated Flow, 142.8-137.74
					Paved Kv= 20.3 fps
1.2	413	0.0040	5.97	42.18	Pipe Channel, 133.7-132
					36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
					n= 0.013 Corrugated PE, smooth interior
4.3	836	Total, I	ncreased t	o minimum	Tc = 6.0 min

Summary for Subcatchment E2b: Southeast - Overland

Runoff	=	1.50 cfs @	12.19 hrs,	Volume=	0.138 af,	Depth= 3.39"
Routed	d to Linl	k DP1 : Spring	Brook			-

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10-YR Rainfall=5.35"

_	Area	(ac) C	N Des	cription					
	0.	108 9	98 Roo	fs, HSG C					
	0.076 89 Gravel roads, HSG C								
	0.095 70 Woods, Good, HSG C								
	0.	194	74 >75°	% Grass c	over, Good	, HSG C			
_	0.	014 9	98 Pave	ed parking	, HSG C				
	0.	487 8	32 Wei	ghted Aver	age				
	0.	365	74.9	5% Pervio	us Area				
	0.	122	25.0	5% Imper	vious Area				
	_								
	ĮĊ	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	9.0	30	0.0150	0.06		Sheet Flow, 140.2-139.75			
						Grass: Bermuda n= 0.410 P2= 3.46"			
	2.6	20	0.1380	0.13		Sheet Flow, 139.75-137			
	07	50	0 0000	4.04		Woods: Light underbrush n= 0.400 P2= 3.46"			
	0.7	50	0.0300	1.21		Shallow Concentrated Flow, 137-135.5			
	0.4	00	0 0070	2.24		Short Grass Pasture KV= 7.0 fps			
	0.1	20	0.0270	3.34		Shallow Concentrated Flow, 138.43-137.74			
	1 2	112	0 0040	5 07	10 10	Paveu $N = 20.3 \text{ Jps}$			
	1.2	413	0.0040	5.97	42.10	26.0" Pound Area 7.1 of Parim 0.4 r 0.75			
						n = 0.013 Corrugated PE smooth interior			
_	12.6	520	Total						
	13.0	009	rola						

Summary for Link DP1: Spring Brook

Inflow A	vrea =	1.907 ac, 7	7.87% Impervi	ous, Inflow [Depth = 4.59"	for 10-YR event
Inflow	=	8.36 cfs @	12.09 hrs, Vo	lume=	0.729 af	
Primary	=	8.36 cfs @	12.09 hrs, Vo	lume=	0.729 af, Atte	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

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Time span=0.00-72.0 Runoff by SCS TR-20 Reach routing by Dyn-Stor-Ind me	00 hrs, dt=0.0 method, UH= thod - Pond	5 hrs, 1441 SCS, Weigh routing by D	points ted-CN yn-Stor-Inc	d method	
SubcatchmentE1: North / Central - Drain Ru	unoff Area=1.3 [,]	17 ac 96.05 ⁰	% Imperviou	us Runoff Dep	th=6.17"
Flow	/ Length=543'	Tc=6.0 min	CN=97 Rเ	unoff=8.20 cfs	0.677 af
SubcatchmentE2a: South - Overland Ru	unoff Area=0.10	03 ac 95.15 ⁰	% Imperviou	us Runoff Dep	th=6.17"
Flow	/ Length=836'	Tc=6.0 min	CN=97 Rเ	unoff=0.64 cfs	0.053 af
SubcatchmentE2b: Southeast - Overland Ru	unoff Area=0.48	87 ac 25.05 ⁰	% Imperviou	us Runoff Dep	th=4.48"
Flow I	Length=539' 1	Tc=13.6 min	CN=82 Rเ	unoff=1.97 cfs	0.182 af
Link DP1: Spring Brook			Inf Prim	flow=10.36 cfs nary=10.36 cfs	0.912 af 0.912 af

Total Runoff Area = 1.907 acRunoff Volume = 0.912 afAverage Runoff Depth = 5.74"22.13% Pervious = 0.422 ac77.87% Impervious = 1.485 ac

Summary for Subcatchment E1: North / Central - Drain Infrastructure

Runoff = 8.20 cfs @ 12.09 hrs, Volume= Routed to Link DP1 : Spring Brook 0.677 af, Depth= 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR Rainfall=6.53"

Area	(ac) C	N Dese	cription		
0.	052 7	'4 >75 [°]	% Grass co	over, Good,	, HSG C
0.	287 9	8 Roo	fs, HSG C		
0.	978 9	8 Pave	ed parking	, HSG C	
1.	317 9	7 Weig	ghted Aver	age	
0.	052	3.95	% Perviou	s Area	
1.	265	96.0	5% Imperv	∕ious Area	
			·		
Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.4	50	0.0586	1.91		Sheet Flow, 145.28-142.35
					Smooth surfaces n= 0.011 P2= 3.46"
1.1	209	0.0236	3.12		Shallow Concentrated Flow, 142.35-137.41
					Paved Kv= 20.3 fps
1.3	83	0.0010	1.09	0.38	Pipe Channel, 133.7-133.7
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
					n= 0.013 Corrugated PE, smooth interior
0.6	99	0.0050	2.84	1.55	Pipe Channel, 133.5-133
					10.0" Round Area= 0.5 sf Perim= 2.6' r= 0.21'
					n= 0.013 Corrugated PE, smooth interior
0.8	76	0.0013	1.64	1.28	Pipe Channel, 132.9-132.8
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.1	26	0.0230	6.88	5.40	Pipe Channel, 132.6-132
					12.0" Round Area= 0.8 st Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
4.3	543	Total, I	ncreased t	o minimum	Tc = 6.0 min

Summary for Subcatchment E2a: South - Overland

Runoff = 0.64 cfs @ 12.09 hrs, Volume= 0.053 af, Depth= 6.17" Routed to Link DP1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR Rainfall=6.53"

Area (ac)	CN	Description
0.005	74	>75% Grass cover, Good, HSG C
0.098	98	Paved parking, HSG C
0.103	97	Weighted Average
0.005		4.85% Pervious Area
0.098		95.15% Impervious Area

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Existing HydroCAD Type III 24-hr 25-YR Rainfall=6.53" Printed 8/23/2023 HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC Page 17

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	50	0.0420	1.68		Sheet Flow, 144.9-142.8 Smooth surfaces n= 0.011 P2= 3.46"
2.6	373	0.0140	2.40		Shallow Concentrated Flow, 142.8-137.74
1.2	413	0.0040	5.97	42.18	Pipe Channel, 133.7-132
					n= 0.013 Corrugated PE, smooth interior

836 Total, Increased to minimum Tc = 6.0 min 4.3

Summary for Subcatchment E2b: Southeast - Overland

Runoff	=	1.97 cfs @	12.19 hrs,	Volume=	0.182 af,	Depth= 4.48"
Routed	d to Lin	k DP1 : Spring	Brook			-

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 25-YR Rainfall=6.53"

_	Area	(ac) C	N Des	cription		
	0.108 98 Roofs, HSG C					
	0.076 89 Gravel roads, HSG C			vel roads, l	HSG C	
	0.	095	70 Woo	ods, Good,	HSG C	
	0.	194	74 >75°	% Grass c	over, Good	, HSG C
_	0.	014 9	98 Pave	ed parking	, HSG C	
	0.	487 8	32 Wei	ghted Aver	age	
	0.	365	74.9	5% Pervio	us Area	
	0.	122	25.0	5% Imper	vious Area	
	_					
	ĮĊ	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.0	30	0.0150	0.06		Sheet Flow, 140.2-139.75
						Grass: Bermuda n= 0.410 P2= 3.46"
	2.6	20	0.1380	0.13		Sheet Flow, 139.75-137
	07	50	0 0000	4.04		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.7	50	0.0300	1.21		Shallow Concentrated Flow, 137-135.5
	0.4	20	0 0070	2.24		Short Grass Pasture KV= 7.0 fps
	0.1	20	0.0270	3.34		Shallow Concentrated Flow, 138.43-137.74
	1 2	112	0 0040	5 07	10 10	Paveu $N = 20.3 \text{ Jps}$
	1.2	413	0.0040	5.97	42.10	26.0" Pound Area 7.1 of Parim 0.4 r 0.75
						n = 0.013 Corrugated PE smooth interior
_	12.6	520	Total			
	13.0	009	rola			

Summary for Link DP1: Spring Brook

Inflow /	Area	=	1.907 ac, 7	7.87% Impe	ervious,	Inflow Depth =	5.7	4" for 25-YR event
Inflow		=	10.36 cfs @	12.09 hrs,	Volume	= 0.912	2 af	
Primar	у	=	10.36 cfs @	12.09 hrs,	Volume	= 0.912	af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

REV0 - W211263-EX Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions	Type III 24-hr	Existing HydroCAD 100-YR Rainfall=9.03" Printed 8/23/2023 Page 19
Time span=0.00-72.00 hrs, dt=0.05 hrs Runoff by SCS TR-20 method, UH=SCS Reach routing by Dyn-Stor-Ind method - Pond routi	, 1441 points , Weighted-CN ng by Dyn-Stor-I	nd method
SubcatchmentE1: North / Central - Drain Runoff Area=1.317 ac	96.05% Impervi	ous Runoff Depth=8.67"
Flow Length=543' Tc=6.	0 min CN=97 R	unoff=11.38 cfs 0.951 af
SubcatchmentE2a: South - Overland Runoff Area=0.103 ac	95.15% Impervi	ous Runoff Depth=8.67"
Flow Length=836' Tc=6	6.0 min CN=97	Runoff=0.89 cfs 0.074 af
SubcatchmentE2b: Southeast - Overland Runoff Area=0.487 ac	25.05% Impervie	ous Runoff Depth=6.84"
Flow Length=539' Tc=13	8.6 min CN=82	Runoff=2.96 cfs 0.278 af
Link DP1: Spring Brook	ا Pr	nflow=14.58 cfs 1.304 af imary=14.58 cfs 1.304 af

Total Runoff Area = 1.907 acRunoff Volume = 1.304 afAverage Runoff Depth = 8.20"22.13% Pervious = 0.422 ac77.87% Impervious = 1.485 ac

Summary for Subcatchment E1: North / Central - Drain Infrastructure

Runoff = 11.38 cfs @ 12.09 hrs, Volume= Routed to Link DP1 : Spring Brook 0.951 af, Depth= 8.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area	(ac) C	N Dese	cription		
0.	052 7	′4 >75°	% Grass co	over, Good,	HSG C
0.1	287 9	8 Roo	fs, HSG C		
0.	978 9	8 Pave	ed parking	, HSG C	
1.	317 9	7 Weig	ghted Aver	age	
0.	052	3.95	% Perviou	s Area	
1.	265	96.0	5% Imperv	/ious Area	
			•		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
0.4	50	0.0586	1.91		Sheet Flow, 145.28-142.35
					Smooth surfaces n= 0.011 P2= 3.46"
1.1	209	0.0236	3.12		Shallow Concentrated Flow, 142.35-137.41
					Paved Kv= 20.3 fps
1.3	83	0.0010	1.09	0.38	Pipe Channel, 133.7-133.7
					8.0" Round Area= 0.3 sf Perim= 2.1' r= 0.17'
					n= 0.013 Corrugated PE, smooth interior
0.6	99	0.0050	2.84	1.55	Pipe Channel, 133.5-133
					10.0" Round Area= 0.5 sf Perim= 2.6' r= 0.21'
					n= 0.013 Corrugated PE, smooth interior
0.8	76	0.0013	1.64	1.28	Pipe Channel, 132.9-132.8
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
0.1	26	0.0230	6.88	5.40	Pipe Channel, 132.6-132
					12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25'
					n= 0.013 Corrugated PE, smooth interior
4.3	543	Total, I	ncreased t	o minimum	Tc = 6.0 min

545 Total, increased to minimum TC – 0.0 min

Summary for Subcatchment E2a: South - Overland

Runoff = 0.89 cfs @ 12.09 hrs, Volume= 0.074 af, Depth= 8.67" Routed to Link DP1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area (ac)	CN	Description
0.005	74	>75% Grass cover, Good, HSG C
0.098	98	Paved parking, HSG C
0.103	97	Weighted Average
0.005		4.85% Pervious Area
0.098		95.15% Impervious Area

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Existing HydroCAD Type III 24-hr 100-YR Rainfall=9.03" Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC Printed 8/23/2023 Page 21

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.5	50	0.0420	1.68		Sheet Flow, 144.9-142.8
					Smooth surfaces n= 0.011 P2= 3.46"
2.6	373	0.0140	2.40		Shallow Concentrated Flow, 142.8-137.74
					Paved Kv= 20.3 fps
1.2	413	0.0040	5.97	42.18	Pipe Channel, 133.7-132
					36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'
					n= 0.013 Corrugated PE, smooth interior
4.3	836	Total, I	ncreased t	o minimum	Tc = 6.0 min

Summary for Subcatchment E2b: Southeast - Overland

Runoff	=	2.96 cfs @	12.18 hrs,	Volume=	0.278 af,	Depth= 6.84"
Routed	d to Lir	nk DP1 : Spring	Brook			

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 100-YR Rainfall=9.03"

_	Area	(ac) C	N Des	cription		
	0.108 98 Roofs, HSG C					
	0.076 89 Gravel roads, HSG C			vel roads, l	HSG C	
	0.	095	70 Woo	ods, Good,	HSG C	
	0.	194	74 >75°	% Grass c	over, Good	, HSG C
_	0.	014 9	98 Pave	ed parking	, HSG C	
	0.	487 8	32 Wei	ghted Aver	age	
	0.	365	74.9	5% Pervio	us Area	
	0.	122	25.0	5% Imper	vious Area	
	_		<u> </u>			
	ĮĊ	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	9.0	30	0.0150	0.06		Sheet Flow, 140.2-139.75
						Grass: Bermuda n= 0.410 P2= 3.46"
	2.6	20	0.1380	0.13		Sheet Flow, 139.75-137
	07	50	0 0000	4.04		Woods: Light underbrush n= 0.400 P2= 3.46"
	0.7	50	0.0300	1.21		Shallow Concentrated Flow, 137-135.5
	0.4	00	0 0070	2.24		Short Grass Pasture KV= 7.0 fps
	0.1	20	0.0270	3.34		Shallow Concentrated Flow, 138.43-137.74
	1 2	112	0 0040	5 07	10 10	Paveu $N = 20.3 \text{ Jps}$
	1.2	413	0.0040	5.97	42.10	26.0" Pound Area 7.1 of Parim 0.4 r 0.75
						n = 0.013 Corrugated PE smooth interior
_	12.6	520	Total			
	13.0	009	rola			

Summary for Link DP1: Spring Brook

 Inflow Area =
 1.907 ac, 77.87% Impervious, Inflow Depth =
 8.20" for 100-YR event

 Inflow =
 14.58 cfs @
 12.09 hrs, Volume=
 1.304 af

 Primary =
 14.58 cfs @
 12.09 hrs, Volume=
 1.304 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

APPENDIX E: PROPOSED CONDITIONS HYDROLOGIC ANALYSIS

- > <u>PROPOSED CONDITIONS DRAINAGE MAP</u>
- > DRAINAGE AREA INLET MAP
- > <u>PROPOSED CONDITIONS HYDROCAD CALCULATIONS</u>











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_	Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
	1	2-YR	Type III 24-hr		Default	24.00	1	3.46	2
	2	10-YR	Type III 24-hr		Default	24.00	1	5.35	2
	3	25-YR	Type III 24-hr		Default	24.00	1	6.53	2
	4	100-YR	Type III 24-hr		Default	24.00	1	9.03	2

Rainfall Events Listing

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Area Listing (selected nodes)

	Area	CN	Description
(a	acres)		(subcatchment-numbers)
	0.234	74	>75% Grass cover, Good, HSG C (P1, P2, P3, P4, P5, P6a)
	1.107	98	Paved parking, HSG C (P1, P2, P3, P4, P5, P6a)
	0.566	98	Roofs, HSG C (P3, P4, P6b)
	1.907	95	TOTAL AREA

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Soil Listing (selected nodes)

Area	Soil	Subcatchment
 (acres)	Group	Numbers
0.000	HSG A	
0.000	HSG B	
1.907	HSG C	P1, P2, P3, P4, P5, P6a, P6b
0.000	HSG D	
0.000	Other	
1.907		TOTAL AREA

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			0.				•)	
	HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
-	0.000	0.000	0.234	0.000	0.000	0.234	>75% Grass cover, Good	P1, P2, P3, P4,
	0.000	0.000	1.107	0.000	0.000	1.107	Paved parking	P5, P6a P1, P2, P3, P4,
	0.000	0.000	0.566	0.000	0.000	0.566	Roofs	P5, P6a P3, P4, P6b
	0.000	0.000	1.907	0.000	0.000	1.907	TOTAL AREA	

Ground Covers (selected nodes)

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Pipe Listing (selected nodes)

Line#	Node	In-Invert	Out-Invert	Length	Slope	n	Width	Diam/Height	Inside-Fill
	numper	(ieel)	(ieet)	(leet)	(1011)		(inches)	(inches)	(incries)
1	#1	135.50	135.70	17.0	-0.0118	0.013	0.0	12.0	0.0
2	#2	135.00	134.00	183.0	0.0055	0.013	0.0	15.0	0.0
3	#3	136.50	136.05	11.5	0.0391	0.013	0.0	12.0	0.0
4	#4	135.00	134.00	74.0	0.0135	0.013	0.0	15.0	0.0

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Prepared by Bohler Eng	ineers			• =	Printed 8	/30/2023
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Reach routir	Time span=0.00-7 Runoff by SCS TR- ng by Dyn-Stor-Ind	72.00 hrs, dt=0.0 20 method, UH: method - Ponc)1 hrs, 7201 =SCS, Weigh I routing by D	ooints ted-CN yn-Stor-Inc	d method	
SubcatchmentP1: South	Edge - Overland F	Runoff Area=0.0 Now Length=394	088 ac 42.059 Tc=6.0 min	% Imperviou CN=84 Rเ	is Runoff Dep unoff=0.20 cfs	oth=1.90" 0.014 af
SubcatchmentP2: South	Central	Runoff Area=0.1	40 ac 95.009 Tc=6.0 min	% Imperviou CN=97 Rเ	is Runoff Dep unoff=0.46 cfs	oth=3.11" 0.036 af
SubcatchmentP3: East		Runoff Area=0.4	65 ac 87.749 Tc=6.0 min	% Imperviou CN=95 Rเ	is Runoff Dep unoff=1.49 cfs	oth=2.90" 0.112 af
SubcatchmentP4: North		Runoff Area=0.4	49 ac 92.659 Tc=6.0 min	% Imperviou CN=96 Rเ	is Runoff Dep unoff=1.47 cfs	oth=3.01" 0.112 af
SubcatchmentP5: North	east	Runoff Area=0.1	97 ac 85.289 Tc=6.0 min	% Imperviou CN=94 Rเ	ls Runoff Dep unoff=0.62 cfs	oth=2.80" 0.046 af
SubcatchmentP6a: Nort	hwest	Runoff Area=0.3	362 ac 84.259 Tc=6.0 min	% Imperviou CN=94 Rเ	ls Runoff Dep unoff=1.13 cfs	oth=2.80" 0.084 af
SubcatchmentP6b: Nort	hwest (Roof)	Runoff Area=0.20	06 ac 100.009 Tc=6.0 min	% Imperviou CN=98 Rเ	ls Runoff Dep unoff=0.69 cfs	oth=3.23" 0.055 af
Reach R1: Spring Brook				lı Ou	nflow=3.50 cfs tflow=3.50 cfs	0.176 af 0.176 af
Reach R2: East Street				lı Ou	nflow=0.66 cfs tflow=0.66 cfs	0.040 af 0.040 af
Pond #1: SWM #1		Peak Elev=1	37.61' Storage	e=453 cf Ir Ou	nflow=0.46 cfs tflow=0.46 cfs	0.036 af 0.026 af
Pond #2: SWM #2	Discarded=0.04 cfs	Peak Elev=136 0.063 af Prima	6.93' Storage= ry=1.35 cfs_0.	:1,045 cf Ir 050 af Out	nflow=1.49 cfs flow=1.39 cfs	0.112 af 0.112 af
Pond #3: SWM #3	Discarded=0.16 cfs	Peak Elev=136 0.101 af Prima	6.86' Storage= ry=0.24 cfs 0.	:1,370 cf Ir 011 af Out	nflow=1.47 cfs flow=0.40 cfs	0.112 af 0.112 af
Pond #4: SWM #4	Discarded=0.04 cfs	Peak Elev=137 0.071 af Prima	′.50' Storage= ry=1.58 cfs_0.	:1,240 cf Ir 069 af Out	nflow=1.82 cfs flow=1.62 cfs	0.140 af 0.140 af
Link DP1: Spring Brook				lı Pri	nflow=4.14 cfs mary=4.14 cfs	0.216 af 0.216 af
Total Rui	noff Area = 1.907 a	ac Runoff Volu 12.27% Perviou	ume = 0.461 s = 0.234 ac	af Averaç 87.73%	ge Runoff De Impervious	pth = 2.90" = 1.673 ac

Summary for Subcatchment P1: South Edge - Overland

Runoff	=	0.20 cfs @	12.09 hrs,	Volume=	0.014 af,	Depth=	1.90"
Routed	d to Rea	ch R2 : East S	Street			-	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area (a	<u>c) C</u>	N De	scription		
0.05	51 7	'4	5% Grass c	over, Good,	HSG C
0.03	37 9	8 Pa	ved parking	, HSG C	
30.0	38 8	4 We	eighted Aver	age	
0.05	51	57.	.95% Pervio	us Area	
0.03	37	42.	.05% Imperv	/ious Area	
Tc L (min)	ength (feet)	Slope (ft/ft)	e Velocity) (ft/sec)	Capacity (cfs)	Description
0.6	50	0.0260) 1.38		Sheet Flow, 143.3-142
2.6	344	0.0120) 2.22		Smooth surfaces n= 0.011 P2= 3.46" Shallow Concentrated Flow, 142-137.74 Paved Kv= 20.3 fps
3.2	394	Total,	Increased t	o minimum	Tc = 6.0 min

Summary for Subcatchment P2: South Central

Runoff 0.46 cfs @ 12.08 hrs, Volume= = Routed to Pond #1 : SWM #1

0.036 af, Depth= 3.11"

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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area (a	ac)	CN	Desc	ription			
0.1	33	98	Pave	d parking,	HSG C		
0.0	07	74	>75%	6 Grass co	over, Good	I, HSG C	
0.1	40	97	Weig	hted Aver	age		
0.0	07		5.00	% Perviou	s Area		
0.1	33		95.00	0% Imperv	vious Area		
Та	المصحية ا			Valacity	Consolt	Description	
	Lengu	ຸ ະ ໂ	Slope	velocity	Capacity	Description	
(min)	(teet)	(TT/ft)	(IT/SEC)	(cfs)		_
6.0						Direct Entry.	

Direct Entry,

Summary for Subcatchment P3: East

1.49 cfs @ 12.08 hrs, Volume= Runoff = Routed to Pond #2 : SWM #2

0.112 af, Depth= 2.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

W211263 Proposed HydroCAD *Type III 24-hr 2-YR Rainfall=3.46"* Printed 8/30/2023 ns LLC Page 9

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Area (a	ac)	CN	Desc	cription		
0.2	211	98	Pave	ed parking	, HSG C	
0.1	97	98	Roof	s, HSG Č		
0.0)57	74	>75%	% Grass co	over, Good	d, HSG C
0.4	65	95	Weig	ghted Aver	age	
0.0)57		12.2	6% Pervio	us Area	
0.4	80		87.74	4% Imper	vious Area	
Tc (min)	Lengt (feet	h S :)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0						Direct Entry,

Summary for Subcatchment P4: North

Runoff = 1.47 cfs @ 12.08 hrs, Volume= Routed to Pond #3 : SWM #3 0.112 af, Depth= 3.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

Are	a (ac)	CN	Desci	ription		
	0.253	98	Pave	d parking	HSG C	
	0.163	98	Roofs	s, HSG C		
	0.033	74	>75%	Grass co	over, Good	d, HSG C
	0.449	96	Weigl	hted Aver	age	
	0.033		7.35%	6 Perviou	s Ārea	
	0.416		92.65	% Imperv	vious Area	
_					•	
Т	c Leng	jth S	Slope	Velocity	Capacity	Description
(min) (fee	et)	<u>(ft/ft)</u>	(ft/sec)	(cfs)	
6.0)					Direct Entry,

Summary for Subcatchment P5: Northeast

Runoff = 0.62 cfs @ 12.08 hrs, Volume= 0.046 af, Depth= 2.80" Routed to Reach R1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area (ac)	CN	Description
0.168	98	Paved parking, HSG C
0.029	74	>75% Grass cover, Good, HSG C
0.197	94	Weighted Average
0.029		14.72% Pervious Area
0.168		85.28% Impervious Area
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--	---------------------------------	
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Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)		
6.0 Direct Entry,		
Summary for Subcatchment P6	a: Northwest	
Runoff = 1.13 cfs @ 12.08 hrs, Volume= 0.084 Routed to Pond #4 : SWM #4	1 af, Depth= 2.80"	
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Spa Type III 24-hr 2-YR Rainfall=3.46"	n= 0.00-72.00 hrs, dt= 0.01 hrs	
Area (ac) CN Description		
0.305 98 Paved parking, HSG C		
0.057 74 >75% Grass cover, Good, HSG C		
0.362 94 Weighted Average		
0.057 15.75% Pervious Area		
0.305 84.25% Impervious Area		
Tc Length Slope Velocity Capacity Description (min) (feet) (ft/ft) (ft/sec) (cfs)		

6.0

Direct Entry,

Summary for Subcatchment P6b: Northwest (Roof)

Runoff 0.69 cfs @ 12.08 hrs, Volume= = Routed to Pond #4 : SWM #4

0.055 af, Depth= 3.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 2-YR Rainfall=3.46"

Area (ac)	CN	Desc	cription		
0.206	98	Root	fs, HSG C		
0.206		100.	00% Impe	rvious Area	a
Tc Leng (min) (fe	gth et)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Reach R1: Spring Brook

Inflow Area = 1.679 ac, 89.52% Impervious, Inflow Depth = 1.26" for 2-YR event 3.50 cfs @ 12.11 hrs, Volume= Inflow = 0.176 af 3.50 cfs @ 12.11 hrs, Volume= 0.176 af, Atten= 0%, Lag= 0.0 min Outflow = Routed to Link DP1 : Spring Brook

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Reach R2: East Street

 Inflow Area =
 0.228 ac, 74.56% Impervious, Inflow Depth =
 2.12" for 2-YR event

 Inflow =
 0.66 cfs @
 12.09 hrs, Volume=
 0.040 af

 Outflow =
 0.66 cfs @
 12.09 hrs, Volume=
 0.040 af, Atten= 0%, Lag= 0.0 min

 Routed to Link DP1 : Spring Brook
 Spring Brook
 0.040 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Pond #1: SWM #1

Inflow Area	a =	0.140 ac, 9	5.00% Impe	ervious, Inflow D	Depth = 3.1	11" for 2-Y	R event
Inflow	=	0.46 cfs @	12.08 hrs,	Volume=	0.036 af		
Outflow	=	0.46 cfs @	12.09 hrs,	Volume=	0.026 af,	Atten= 0%,	Lag= 0.4 min
Primary	=	0.46 cfs @	12.09 hrs,	Volume=	0.026 af		•
Routed	to Reac	h R2 : East S	Street				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.61' @ 12.09 hrs Surf.Area= 281 sf Storage= 453 cf

Plug-Flow detention time= 160.6 min calculated for 0.026 af (72% of inflow) Center-of-Mass det. time= 71.3 min (835.4 - 764.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	283 cf	15.75'W x 17.86'L x 3.50'H Field A
			984 cf Overall - 276 cf Embedded = 709 cf x 40.0% Voids
#2A	135.50'	276 cf	ADS_StormTech SC-740 +Cap x 6 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			6 Chambers in 3 Rows
		559 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.70'	12.0" Round Culvert
	-		L= 17.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.50' / 135.70' S= -0.0118 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	137.50'	4.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.46 cfs @ 12.09 hrs HW=137.61' TW=0.00' (Dynamic Tailwater)

2=Sharp-Crested Rectangular Weir (Weir Controls 0.46 cfs @ 1.08 fps)

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Summary for Pond #2: SWM #2

Inflow Area = 0.465 ac, 87.74% Impervious, Inflow Depth = 2.90" for 2-YR event 1.49 cfs @ 12.08 hrs, Volume= Inflow = 0.112 af Outflow = 1.39 cfs @ 12.11 hrs, Volume= 0.112 af, Atten= 6%, Lag= 1.8 min Discarded = 0.04 cfs @ 9.30 hrs, Volume= 0.063 af Primary = 1.35 cfs @ 12.11 hrs, Volume= 0.050 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 136.93' @ 12.11 hrs Surf.Area= 658 sf Storage= 1,045 cf

Plug-Flow detention time= 131.4 min calculated for 0.112 af (100% of inflow) Center-of-Mass det. time= 131.4 min (910.0 - 778.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	627 cf	20.50'W x 32.10'L x 3.50'H Field A
			2,303 cf Overall - 735 cf Embedded = 1,568 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 4 Rows
		1,362 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 183.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.50'	20.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 9.30 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=1.35 cfs @ 12.11 hrs HW=136.93' TW=0.00' (Dynamic Tailwater) 1=Culvert (Passes 1.35 cfs of 5.14 cfs potential flow) 2=Orifice/Grate (Orifice Controls 1.35 cfs @ 2.43 fps)

-2=Orifice/Grate (Onfice Controls 1.35 0.3 (2.10.1-7) -3=Sharp-Crested Rectangular Weir(Controls 0.00 cfs) Page 12

W211263 Proposed HydroCAD Type III 24-hr 2-YR Rainfall=3.46" **REV0 - W211263-PR** Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC

Summary for Pond #3: SWM #3

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Inflow Area = 0.449 ac, 92.65% Impervious, Inflow Depth = 3.01" for 2-YR event 1.47 cfs @ 12.08 hrs, Volume= Inflow = 0.112 af Outflow = 0.40 cfs @ 12.43 hrs, Volume= 0.112 af, Atten= 73%, Lag= 20.8 min Discarded = 0.16 cfs @ 11.66 hrs, Volume= 0.101 af Primary = 0.24 cfs @ 12.43 hrs, Volume= 0.011 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 136.86' @ 12.43 hrs Surf.Area= 2,840 sf Storage= 1,370 cf

Plug-Flow detention time= 42.4 min calculated for 0.112 af (100% of inflow) Center-of-Mass det. time= 42.4 min (814.3 - 771.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	136.00'	2,002 cf	34.83'W x 81.52'L x 2.33'H Field A
			6,626 cf Overall - 1,622 cf Embedded = 5,004 cf x 40.0% Voids
#2A	136.50'	1,622 cf	ADS_StormTech SC-310 +Cap x 110 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			110 Chambers in 10 Rows
		3,623 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	136.50'	12.0" Round Culvert
	-		L= 11.5' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 136.50' / 136.05' S= 0.0391 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	136.70'	14.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.83'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	136.00'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.16 cfs @ 11.66 hrs HW=136.03' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.16 cfs)

Primary OutFlow Max=0.24 cfs @ 12.43 hrs HW=136.86' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 0.24 cfs of 0.41 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.24 cfs @ 1.29 fps) **3=Sharp-Crested Rectangular Weir**(Controls 0.00 cfs)

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Summary for Pond #4: SWM #4

Inflow Area = 0.568 ac, 89.96% Impervious, Inflow Depth = 2.95" for 2-YR event 1.82 cfs @ 12.08 hrs, Volume= Inflow = 0.140 af Outflow = 1.62 cfs @ 12.13 hrs, Volume= 0.140 af, Atten= 11%, Lag= 2.5 min Discarded = 0.04 cfs @ 8.76 hrs, Volume= 0.071 af Primary = 1.58 cfs @ 12.13 hrs, Volume= 0.069 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.50' @ 12.13 hrs Surf.Area= 666 sf Storage= 1,240 cf

Plug-Flow detention time= 136.0 min calculated for 0.140 af (100% of inflow) Center-of-Mass det. time= 136.0 min (908.8 - 772.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	639 cf	11.00'W x 60.58'L x 3.50'H Field A
			2,332 cf Overall - 735 cf Embedded = 1,597 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 2 Rows
		1.374 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 74.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0135 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.75'	20.0" W x 3.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 8.76 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=1.58 cfs @ 12.13 hrs HW=137.50' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 1.58 cfs of 6.38 cfs potential flow) **1=Culvert** (Orifice Controls 1.58 cfs @ 2.70 fps)

2=Orifice/Grate (Orifice Controls 1.58 cfs @ 3.79 fps) **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs) Page 14

Summary for Link DP1: Spring Brook

Inflow Ar	ea =	1.907 ac, 8	7.73% Impervious,	Inflow Depth =	1.36" for 2	2-YR event
Inflow	=	4.14 cfs @	12.11 hrs, Volume	e= 0.216 a	af	
Primary	=	4.14 cfs @	12.11 hrs, Volume	e= 0.216 a	af, Atten= 0%	%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

REV0 - W211263-PR			Type	W21126	∃ Proposed 10-YR Rain	lydroCAD fall=5.35"
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l Reach routir	Time span=0.00- Runoff by SCS TR- ng by Dyn-Stor-Ind	72.00 hrs, dt=0.0 20 method, UH= method - Pond)1 hrs, 7201 =SCS, Weigh routing by D	ooints ted-CN yn-Stor-Ir	nd method	
SubcatchmentP1: South	Edge - Overland F	Runoff Area=0.0 Flow Length=394'	88 ac 42.05 Tc=6.0 min	% Impervic CN=84 F	ous Runoff De Runoff=0.37 cfs	pth=3.59" 5_0.026 af
SubcatchmentP2: South	Central	Runoff Area=0.1	40 ac 95.00° Tc=6.0 min	% Impervic CN=97 F	ous Runoff De Runoff=0.73 cfs	pth=5.00" 5_0.058 af
SubcatchmentP3: East		Runoff Area=0.4	65 ac 87.74 Tc=6.0 min	% Impervic CN=95 F	ous Runoff De Runoff=2.38 cfs	pth=4.77" s_0.185 af
SubcatchmentP4: North		Runoff Area=0.4	49 ac 92.65° Tc=6.0 min	% Impervic CN=96 F	ous Runoff De Runoff=2.32 cfs	pth=4.88" s_0.183 af
SubcatchmentP5: North	east	Runoff Area=0.1	97 ac 85.28 Tc=6.0 min	% Impervic CN=94 F	ous Runoff De Runoff=0.99 cfs	pth=4.65" s_0.076 af
SubcatchmentP6a: North	hwest	Runoff Area=0.3	62 ac 84.25 Tc=6.0 min	% Impervic CN=94 F	ous Runoff De Runoff=1.83 cfs	pth=4.65" § 0.140 af
SubcatchmentP6b: Nort	hwest (Roof)	Runoff Area=0.20	6 ac 100.00 Tc=6.0 min	% Impervic CN=98 F	ous Runoff De Runoff=1.08 cfs	pth=5.11" s_0.088 af
Reach R1: Spring Brook				0	Inflow=6.39 cfs outflow=6.39 cfs	s 0.380 af s 0.380 af
Reach R2: East Street				0	Inflow=1.09 cfs outflow=1.09 cfs	s 0.075 af s 0.075 af
Pond #1: SWM #1		Peak Elev=1	37.65' Storag	e=458 cf O	Inflow=0.73 cfs outflow=0.73 cfs	s 0.058 af s 0.048 af
Pond #2: SWM #2	Discarded=0.04 cfs	Peak Elev=137 0.074 af Prima	7.30' Storage= ry=2.12 cfs_0.	:1,174 cf 111 af Ou	Inflow=2.38 cfs utflow=2.15 cfs	o.185 af 0.185 af
Pond #3: SWM #3	Discarded=0.16 cfs	Peak Elev=137 0.136 af Prima	′.11' Storage= ry=0.91 cfs_0.	:1,893 cf 047 af Ou	Inflow=2.32 cfs utflow=1.07 cfs	s 0.183 af 0.183 af
Pond #4: SWM #4	Discarded=0.04 cfs	Peak Elev=137 0.082 af Prima	7.69' Storage= ry=2.86 cfs_0.	:1,291 cf 146 af Ou	Inflow=2.91 cfs utflow=2.89 cfs	o.228 af 0.228 af
Link DP1: Spring Brook				Р	Inflow=7.45 cfs rimary=7.45 cfs	s 0.455 af s 0.455 af
Total Rur	noff Area = 1.907 a	ac Runoff Volu 12.27% Perviou	ıme = 0.756 s = 0.234 ac	af Avera 87.73%	age Runoff D % Impervious	epth = 4.76" s = 1.673 ac

Summary for Subcatchment P1: South Edge - Overland

Runoff	=	0.37 cfs @	12.09 hrs,	Volume=	0.026 af,	Depth=	3.59"
Routed	to Read	ch R2 : East S	Street			-	

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area	(ac) (CN D	escription		
0.	051	74 >7	′5% Grass c	over, Good,	, HSG C
0.	037	98 Pa	aved parking	, HSG C	
0.	088	84 W	eighted Ave	rage	
0.	051	57	.95% Pervic	us Area	
0.	037	42	2.05% Imper	vious Area	
Tc (min)	Length (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
0.6	50	0.026	0 1.38		Sheet Flow, 143.3-142
2.6	344	0.012	2.22		Smooth surfaces n= 0.011 P2= 3.46" Shallow Concentrated Flow, 142-137.74 Paved Kv= 20.3 fps
3.2	394	Total	Increased	to minimum	Tc = 6.0 min

Summary for Subcatchment P2: South Central

Runoff 0.73 cfs @ 12.08 hrs, Volume= = Routed to Pond #1 : SWM #1

0.058 af, Depth= 5.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area (ac	c) CN	Descri	iption			
0.13	3 98	Paved	l parking,	HSG C		
0.00	7 74	>75%	Grass co	over, Good	HSG C	
0.14	0 97	Weigh	ted Aver	age		
0.00	7	5.00%	Perviou	s Area		
0.13	3	95.009	% Imperv	rious Area		
To Le	enath	Slone \	Velocity	Canacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description	
6.0	(····)	()	()	(0.0)	Direct Entry.	

Direct Entry,

Summary for Subcatchment P3: East

2.38 cfs @ 12.08 hrs, Volume= Runoff = Routed to Pond #2 : SWM #2

0.185 af, Depth= 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

W211263 Proposed HydroCAD *Type III 24-hr 10-YR Rainfall=5.35"* Printed 8/30/2023 tions LLC Page 18

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Area (ac)	CN	Desc	ription			
0.2	211	98	Pave	d parking	HSG C		
0.1	197	98	Roof	s, HSG C			
0.0)57	74	>75%	6 Grass co	over, Good	d, HSG C	
0.4	465	95	Weig	hted Aver	age		
0.0)57		12.2	5% Pervio	us Area		
0.4	408		87.74	4% Imperv	vious Area		
Tc (min)	Leng (fee	th et)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
6.0						Direct Entry,	

Summary for Subcatchment P4: North

Runoff = 2.32 cfs @ 12.08 hrs, Volume= Routed to Pond #3 : SWM #3 0.183 af, Depth= 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

	Area (ac)	CN	Descri	ption		
	0.253	98	Paved	parking,	HSG C	
	0.163	98	Roofs,	HSG C		
	0.033	74	>75%	Grass co	over, Good	d, HSG C
	0.449	96	Weigh	ted Aver	age	
	0.033		7.35%	Perviou	s Ārea	
	0.416		92.659	% Imper∖	vious Area	
	т ,				O	
,	IC Leng	ith E	slope \	Velocity	Capacity	Description
(min) (fee	et)	(ft/ft)	(ft/sec)	(cts)	
	6.0					Direct Entry,

Summary for Subcatchment P5: Northeast

Runoff = 0.99 cfs @ 12.08 hrs, Volume= 0.076 af, Depth= 4.65" Routed to Reach R1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area (ac)	CN	Description
0.168	98	Paved parking, HSG C
0.029	74	>75% Grass cover, Good, HSG C
0.197	94	Weighted Average
0.029		14.72% Pervious Area
0.168		85.28% Impervious Area

REV0 -	W2112	63-PR				Туре	e III 24-hr 1	0-YR Rainfall=5.35"
Prepare	d by Boł	ler Engi	neers					Printed 8/30/2023
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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry	/,		
		:	Summar	y for Sub	ocatchmen	t P6a: Nor	thwest	
Runoff Route	unoff = 1.83 cfs @ 12.08 hrs, Volume= 0.140 af, Depth= 4.65" Routed to Pond #4 : SWM #4							
Runoff b Type III :	y SCS TF 24-hr 10-	R-20 meth YR Rainf	nod, UH=S fall=5.35"	SCS, Weigh	ited-CN, Time	e Span= 0.00	0-72.00 hrs,	dt= 0.01 hrs
Area	(ac) C	N Desc	cription					
0. 0.	.305 9 .057 7	8 Pave 4 >75%	ed parking % Grass c	, HSG C over, Good	, HSG C			
0. 0. 0.	.362 9 .057 .305	4 Weig 15.7 84.2	hted Aver 5% Pervio 5% Imper	rage ous Area vious Area				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			

Summary for Subcatchment P6b: Northwest (Roof)

Direct Entry,

Runoff 1.08 cfs @ 12.08 hrs, Volume= = Routed to Pond #4 : SWM #4

6.0

0.088 af, Depth= 5.11"

W211263 Proposed HydroCAD

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 10-YR Rainfall=5.35"

Area (ac)	CN	Desc	cription		
0.206	98	Roof	fs, HSG C		
0.206		100.	00% Impe	rvious Area	a
Tc Ler (min) (fe	ngth eet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Reach R1: Spring Brook

Inflow Area = 1.679 ac, 89.52% Impervious, Inflow Depth = 2.72" for 10-YR event Inflow = 6.39 cfs @ 12.11 hrs, Volume= 0.380 af 6.39 cfs @ 12.11 hrs, Volume= Outflow 0.380 af, Atten= 0%, Lag= 0.0 min = Routed to Link DP1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Reach R2: East Street

 Inflow Area =
 0.228 ac, 74.56% Impervious, Inflow Depth =
 3.93" for 10-YR event

 Inflow =
 1.09 cfs @
 12.09 hrs, Volume=
 0.075 af

 Outflow =
 1.09 cfs @
 12.09 hrs, Volume=
 0.075 af, Atten= 0%, Lag= 0.0 min

 Routed to Link DP1 : Spring Brook
 Spring Brook
 0.075 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Pond #1: SWM #1

Inflow Area	ı =	0.140 ac, 9	5.00% Impe	ervious, Inflow D)epth = 5.0	00" for 10-`	YR event
Inflow	=	0.73 cfs @	12.08 hrs,	Volume=	0.058 af		
Outflow	=	0.73 cfs @	12.09 hrs,	Volume=	0.048 af,	Atten= 0%,	Lag= 0.3 min
Primary	=	0.73 cfs @	12.09 hrs,	Volume=	0.048 af		•
Routed	to Reac	h R2 : East S	Street				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.65' @ 12.09 hrs Surf.Area= 281 sf Storage= 458 cf

Plug-Flow detention time= 127.7 min calculated for 0.048 af (83% of inflow) Center-of-Mass det. time= 57.5 min (811.8 - 754.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	283 cf	15.75'W x 17.86'L x 3.50'H Field A
			984 cf Overall - 276 cf Embedded = 709 cf x 40.0% Voids
#2A	135.50'	276 cf	ADS_StormTech SC-740 +Cap x 6 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			6 Chambers in 3 Rows
		559 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.70'	12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.50' / 135.70' S= -0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	137.50'	4.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.73 cfs @ 12.09 hrs HW=137.65' TW=0.00' (Dynamic Tailwater) **1=Culvert** (Passes 0.73 cfs of 3.59 cfs potential flow)

2=Sharp-Crested Rectangular Weir (Weir Controls 0.73 cfs @ 1.25 fps)

W211263 Proposed HydroCAD Type III 24-hr 10-YR Rainfall=5.35" **REV0 - W211263-PR** Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC

Summary for Pond #2: SWM #2

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Inflow Area = 0.465 ac, 87.74% Impervious, Inflow Depth = 4.77" for 10-YR event 2.38 cfs @ 12.08 hrs, Volume= Inflow = 0.185 af Outflow = 2.15 cfs @ 12.12 hrs, Volume= 0.185 af, Atten= 9%, Lag= 2.3 min Discarded = 0.04 cfs @ 7.77 hrs, Volume= 0.074 af Primary = 2.12 cfs @ 12.12 hrs, Volume= 0.111 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.30' @ 12.12 hrs Surf.Area= 658 sf Storage= 1,174 cf

Plug-Flow detention time= 103.3 min calculated for 0.185 af (100% of inflow) Center-of-Mass det. time= 103.4 min (869.9 - 766.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	627 cf	20.50'W x 32.10'L x 3.50'H Field A
			2,303 cf Overall - 735 cf Embedded = 1,568 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 4 Rows
		1,362 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 183.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.50'	20.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 7.77 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=2.11 cfs @ 12.12 hrs HW=137.30' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 2.11 cfs of 5.67 cfs potential flow)

2=Orifice/Grate (Orifice Controls 2.11 cfs @ 3.81 fps) **3=Sharp-Crested Rectangular Weir**(Controls 0.00 cfs)

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Summary for Pond #3: SWM #3

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Inflow Area = 0.449 ac, 92.65% Impervious, Inflow Depth = 4.88" for 10-YR event 2.32 cfs @ 12.08 hrs, Volume= Inflow = 0.183 af Outflow = 1.07 cfs @ 12.25 hrs, Volume= 0.183 af, Atten= 54%, Lag= 9.9 min Discarded = 0.16 cfs @ 11.25 hrs, Volume= 0.136 af Primary = 0.91 cfs @ 12.25 hrs, Volume= 0.047 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.11' @ 12.25 hrs Surf.Area= 2,840 sf Storage= 1,893 cf

Plug-Flow detention time= 38.6 min calculated for 0.183 af (100% of inflow) Center-of-Mass det. time= 38.6 min (799.4 - 760.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	136.00'	2,002 cf	34.83'W x 81.52'L x 2.33'H Field A
			6,626 cf Overall - 1,622 cf Embedded = 5,004 cf x 40.0% Voids
#2A	136.50'	1,622 cf	ADS_StormTech SC-310 +Cap x 110 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			110 Chambers in 10 Rows
		3,623 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	136.50'	12.0" Round Culvert
			L= 11.5' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 136.50' / 136.05' S= 0.0391 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	136.70'	14.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.83'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	136.00'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.16 cfs @ 11.25 hrs HW=136.02' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.16 cfs)

Primary OutFlow Max=0.91 cfs @ 12.25 hrs HW=137.11' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 0.91 cfs of 1.06 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.91 cfs @ 2.33 fps) **3=Sharp-Crested Rectangular Weir**(Controls 0.00 cfs)

W211263 Proposed HydroCAD Type III 24-hr 10-YR Rainfall=5.35" **REV0 - W211263-PR** Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC

Summary for Pond #4: SWM #4

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Inflow Area = 0.568 ac, 89.96% Impervious, Inflow Depth = 4.82" for 10-YR event 2.91 cfs @ 12.08 hrs, Volume= Inflow = 0.228 af Outflow = 2.89 cfs @ 12.09 hrs, Volume= 0.228 af, Atten= 0%, Lag= 0.5 min Discarded = 0.04 cfs @ 7.06 hrs, Volume= 0.082 af Primary = 2.86 cfs @ 12.09 hrs, Volume= 0.146 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.69' @ 12.09 hrs Surf.Area= 666 sf Storage= 1,291 cf

Plug-Flow detention time= 104.5 min calculated for 0.228 af (100% of inflow) Center-of-Mass det. time= 104.6 min (866.7 - 762.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	639 cf	11.00'W x 60.58'L x 3.50'H Field A
			2,332 cf Overall - 735 cf Embedded = 1,597 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 2 Rows
		1,374 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 74.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0135 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.75'	20.0" W x 3.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 7.06 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=2.85 cfs @ 12.09 hrs HW=137.69' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 2.85 cfs of 6.70 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.81 cfs @ 4.33 fps)

2=Orifice/Grate (Office Controls 1.01 of the incompany) **3=Sharp-Crested Rectangular Weir** (Weir Controls 1.05 cfs @ 1.41 fps)

Summary for Link DP1: Spring Brook

 Inflow Area =
 1.907 ac, 87.73% Impervious, Inflow Depth =
 2.86" for 10-YR event

 Inflow =
 7.45 cfs @
 12.11 hrs, Volume=
 0.455 af

 Primary =
 7.45 cfs @
 12.11 hrs, Volume=
 0.455 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

REV0 - W211263-PR			Type	W21126 III 24-hr	3 Proposed H	lydroCAD fall=6.53″
Prepared by Bohler Eng	ineers		rype	, ,,, ,, ,,,,	Printed	8/30/2023
HydroCAD® 10.20-2g s/n 0	3478 © 2022 Hydro	CAD Software So	lutions LLC			Page 25
Reach routir	Time span=0.00- Runoff by SCS TR- ng by Dyn-Stor-Ind	72.00 hrs, dt=0.0 20 method, UH: method - Ponc)1 hrs, 7201 =SCS, Weigh I routing by D	points hted-CN)yn-Stor-Ii	nd method	
SubcatchmentP1: South	Edge - Overland F	Runoff Area=0.0 Flow Length=394'	088 ac 42.05 Tc=6.0 min	% Impervio CN=84 F	ous Runoff De Runoff=0.47 cfs	epth=4.69" s_0.034 af
SubcatchmentP2: South	Central	Runoff Area=0.1	40 ac 95.00 Tc=6.0 min	% Impervio CN=97 I	ous Runoff De Runoff=0.89 cfs	epth=6.17" s_0.072 af
SubcatchmentP3: East		Runoff Area=0.4	65 ac 87.74 Tc=6.0 min	% Impervio CN=95 I	ous Runoff De Runoff=2.93 cfs	epth=5.94" s_0.230 af
SubcatchmentP4: North		Runoff Area=0.4	49 ac 92.65 Tc=6.0 min	% Impervio CN=96 I	ous Runoff De Runoff=2.85 cfs	epth=6.06" s_0.227 af
SubcatchmentP5: North	east	Runoff Area=0.1	97 ac 85.28 Tc=6.0 min	% Impervio CN=94 I	ous Runoff De Runoff=1.23 cfs	epth=5.82" s_0.096 af
SubcatchmentP6a: Nort	hwest	Runoff Area=0.3	62 ac 84.25 Tc=6.0 min	% Impervio CN=94 I	ous Runoff De Runoff=2.26 cfs	epth=5.82" s_0.176 af
SubcatchmentP6b: Nort	hwest (Roof)	Runoff Area=0.20	06 ac 100.00 Tc=6.0 min	% Impervio CN=98 I	ous Runoff De Runoff=1.32 cfs	epth=6.29" s_0.108 af
Reach R1: Spring Brook				C	Inflow=8.38 cf outflow=8.38 cf	s 0.517 af s 0.517 af
Reach R2: East Street				C	Inflow=1.37 cf Outflow=1.37 cf	s 0.096 af s 0.096 af
Pond #1: SWM #1		Peak Elev=1	37.67' Storag	e=461 cf C	Inflow=0.89 cfs outflow=0.89 cfs	s 0.072 af s 0.062 af
Pond #2: SWM #2	Discarded=0.04 cfs	Peak Elev=137 0.079 af Prima	′.56' Storage⊧ ry=2.74 cfs_0	=1,247 cf .151 af O	Inflow=2.93 cfs utflow=2.78 cfs	s 0.230 af s 0.230 af
Pond #3: SWM #3	Discarded=0.16 cfs	Peak Elev=137 0.154 af Prima	′.31' Storage⊧ ry=1.24 cfs_0	=2,280 cf .073 af O	Inflow=2.85 cfs utflow=1.40 cfs	s 0.227 af s 0.227 af
Pond #4: SWM #4	Discarded=0.04 cfs	Peak Elev=137 0.086 af Prima	′.75' Storage⊧ ry=3.53 cfs_0	=1,308 cf .198 af O	Inflow=3.58 cfs utflow=3.56 cfs	s 0.284 af s 0.284 af
Link DP1: Spring Brook				Ρ	Inflow=9.72 cf rimary=9.72 cf	s 0.614 af s 0.614 af
Total Rur	noff Area = 1.907 a	ac Runoff Volu 12.27% Perviou	ıme = 0.942 s = 0.234 ac	af Avera 87.739	age Runoff D % Impervious	epth = 5.93" s = 1.673 ac

Summary for Subcatchment P1: South Edge - Overland

Runoff	=	0.47 cfs @	12.09 hrs,	Volume=	0.034 af,	Depth= 4.69"
Routed	I to Re	each R2 : East S	Street			-

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

Area (a	ac) C	N De	scription							
0.0	51 7	74 >7	75% Grass cover, Good, HSG C							
0.0	37 9	98 Pa	aved parking, HSG C							
0.0	0.088 84 Weighted Average									
0.0	51	57	.95% Pervio	us Area						
0.0	37	42	.05% Imperv	/ious Area						
Tc (min)	Length (feet)	Slope (ft/ft	e Velocity) (ft/sec)	Capacity (cfs)	Description					
0.6	50	0.0260	0 1.38		Sheet Flow, 143.3-142					
2.6	344	0.0120	0 2.22		Smooth surfaces n= 0.011 P2= 3.46" Shallow Concentrated Flow, 142-137.74 Paved Kv= 20.3 fps					
3.2	394	Total,	Increased t	o minimum	Tc = 6.0 min					

Summary for Subcatchment P2: South Central

Runoff 0.89 cfs @ 12.08 hrs, Volume= = Routed to Pond #1 : SWM #1

0.072 af, Depth= 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

Area (ac	c) CN	Descri	iption			
0.13	3 98	Paved	l parking,	HSG C		
0.00	7 74	>75%	Grass co	over, Good	HSG C	
0.14	0 97	Weigh	ted Aver	age		
0.00	7	5.00%	Perviou	s Area		
0.133 95.00% Impervious Area						
To Le	enath	Slone \	Velocity	Canacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description	
6.0	(····)	()	()	(0.0)	Direct Entry.	

Direct Entry,

Summary for Subcatchment P3: East

2.93 cfs @ 12.08 hrs, Volume= Runoff = Routed to Pond #2 : SWM #2

0.230 af, Depth= 5.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

W211263 Proposed HydroCAD *Type III 24-hr 25-YR Rainfall=6.53"* Printed 8/30/2023 tions LLC Page 27

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	Area ((ac)	CN	Desc	cription			
	0.2	211	98	Pave	d parking	, HSG C		
	0.	197	98	Roof	s, HSG C			
	0.0	057	74	>75%	6 Grass co	over, Good	, HSG C	
	0.4	465	95	Weig	hted Aver	age		
	0.0	057		12.2	6% Pervio	us Area		
	0.4	0.408 87.74% Impervious Area				ious Area		
	Тс	Leng	th	Slope	Velocity	Capacity	Description	
(min)	(fee	et)	(ft/ft)	(ft/sec)	(cfs)		
	6.0						Direct Entry,	

Summary for Subcatchment P4: North

Runoff = 2.85 cfs @ 12.08 hrs, Volume= Routed to Pond #3 : SWM #3 0.227 af, Depth= 6.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

	Area (ac)	CN	Descrip	otion		
	0.253	98	Paved	parking,	HSG C	
	0.163	98	Roofs,	HSG C		
_	0.033	74	>75% (Grass co	over, Good	d, HSG C
	0.449	96	Weight	ed Aver	age	
	0.033		7.35%	Perviou	s Area	
	0.416		92.65%	6 Imperv	vious Area	1
	T . 1			/ . I ¹ 6	0	Description
,	IC Leng	jth S	slope v	elocity	Capacity	Description
(min) (tee	et)	(ft/ft)	(ft/sec)	(cfs)	
	6.0					Direct Entry,

Summary for Subcatchment P5: Northeast

Runoff = 1.23 cfs @ 12.08 hrs, Volume= 0.096 af, Depth= 5.82" Routed to Reach R1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

Area (ac)	CN	Description
0.168	98	Paved parking, HSG C
0.029	74	>75% Grass cover, Good, HSG C
0.197	94	Weighted Average
0.029		14.72% Pervious Area
0.168		85.28% Impervious Area

REV0 -	W211	263-PR				Туре	III 24-hr_25-YR Rainfall=6.53"
Prepare	d by Bc	hler Eng	ineers				Printed 8/30/2023
HydroCA	.D® 10.20	<u>)-2g_s/n 0</u>	3478 © 202	22 HydroCAI	D Software Solu	tions LLC	Page 28
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
6.0					Direct Entry,		
			Summar	y for Sub	ocatchment	P6a: Nort	hwest
Runoff Route	= ed to Po	2.26 cf nd #4 : SV	s @ 12.0 VM #4	8 hrs, Volu	me= 0.	176 af, Dep	oth= 5.82"
Runoff b Type III :	y SCS T 24-hr 25	⁻ R-20 met 5-YR Rain	hod, UH=S fall=6.53"	SCS, Weigh	nted-CN, Time S	Span= 0.00-	72.00 hrs, dt= 0.01 hrs
Area	(ac) (CN Des	cription				
0.	.305	98 Pav	ed parking	, HSG C			
0.	.057	74 >75	% Grass c	over, Good	, HSG C		
0. 0. 0.	.362 .057 .305	94 Wei 15.7 84.2	ghted Aver 5% Pervic 5% Imper	rage ous Area vious Area			
Тс	Length	Slope	Velocity	Capacity	Description		

Summary for Subcatchment P6b: Northwest (Roof)

Direct Entry,

Runoff = 1.32 cfs @ 12.08 hrs, Volume= Routed to Pond #4 : SWM #4

(ft/sec)

(ft/ft)

(min)

6.0

(feet)

0.108 af, Depth= 6.29"

W211263 Proposed HydroCAD

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 25-YR Rainfall=6.53"

(cfs)

Area (ac)) CN	Desc	cription		
0.206	98	Roof	s, HSG C		
0.206	5	100.	00% Impe	rvious Area	a
Tc Le (min) (ngth feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.0					Direct Entry,

Summary for Reach R1: Spring Brook

Inflow Area = 1.679 ac, 89.52% Impervious, Inflow Depth = 3.70" for 25-YR event Inflow = 8.38 cfs @ 12.11 hrs, Volume= 0.517 af Outflow = 8.38 cfs @ 12.11 hrs, Volume= 0.517 af, Atten= 0%, Lag= 0.0 min Routed to Link DP1 : Spring Brook Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Reach R2: East Street

Inflow Area = 0.228 ac, 74.56% Impervious, Inflow Depth = 5.08" for 25-YR event Inflow = 1.37 cfs @ 12.09 hrs, Volume= 0.096 af Outflow = 1.37 cfs @ 12.09 hrs, Volume= 0.096 af, Atten= 0%, Lag= 0.0 min Routed to Link DP1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Pond #1: SWM #1

Inflow Area	=	0.140 ac, 9	5.00% Impe	ervious, Inflow	Depth = 6.1	7" for 25-	YR event
Inflow	=	0.89 cfs @	12.08 hrs,	Volume=	0.072 af		
Outflow	=	0.89 cfs @	12.09 hrs,	Volume=	0.062 af,	Atten= 0%,	Lag= 0.3 min
Primary	=	0.89 cfs @	12.09 hrs,	Volume=	0.062 af		-
Routed	to Reac	h R2 : East S	Street				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.67' @ 12.09 hrs Surf.Area= 281 sf Storage= 461 cf

Plug-Flow detention time= 113.9 min calculated for 0.062 af (86% of inflow) Center-of-Mass det. time= 51.9 min (802.5 - 750.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	283 cf	15.75'W x 17.86'L x 3.50'H Field A
			984 cf Overall - 276 cf Embedded = 709 cf x 40.0% Voids
#2A	135.50'	276 cf	ADS_StormTech SC-740 +Cap x 6 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			6 Chambers in 3 Rows
		559 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.70'	12.0" Round Culvert
			L= 17.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.50' / 135.70' S= -0.0118 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	137.50'	4.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=0.89 cfs @ 12.09 hrs HW=137.67' TW=0.00' (Dynamic Tailwater)

2=Sharp-Crested Rectangular Weir (Weir Controls 0.89 cfs @ 1.34 fps)

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Summary for Pond #2: SWM #2

Inflow Area = 0.465 ac, 87.74% Impervious, Inflow Depth = 5.94" for 25-YR event 2.93 cfs @ 12.08 hrs, Volume= Inflow = 0.230 af Outflow = 2.78 cfs @ 12.11 hrs, Volume= 0.230 af, Atten= 5%, Lag= 1.7 min Discarded = 0.04 cfs @ 6.93 hrs, Volume= 0.079 af Primary = 2.74 cfs @ 12.11 hrs, Volume= 0.151 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.56' @ 12.11 hrs Surf.Area= 658 sf Storage= 1,247 cf

Plug-Flow detention time= 91.5 min calculated for 0.230 af (100% of inflow) Center-of-Mass det. time= 91.5 min (853.1 - 761.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	627 cf	20.50'W x 32.10'L x 3.50'H Field A
			2,303 cf Overall - 735 cf Embedded = 1,568 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 4 Rows
		1,362 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 183.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.50'	20.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 6.93 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=2.73 cfs @ 12.11 hrs HW=137.56' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 2.73 cfs of 6.03 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 2.53 cfs @ 4.55 fps)

-2=Orifice/Grate (Office Controls 2.00 of the first and first) -3=Sharp-Crested Rectangular Weir (Weir Controls 0.21 cfs @ 0.82 fps)

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W211263 Proposed HydroCAD Type III 24-hr 25-YR Rainfall=6.53" **REV0 - W211263-PR** Prepared by Bohler Engineers HydroCAD® 10.20-2g s/n 03478 © 2022 HydroCAD Software Solutions LLC

Summary for Pond #3: SWM #3

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Inflow Area = 0.449 ac, 92.65% Impervious, Inflow Depth = 6.06" for 25-YR event 2.85 cfs @ 12.08 hrs, Volume= Inflow = 0.227 af Outflow = 1.40 cfs @ 12.23 hrs, Volume= 0.227 af, Atten= 51%, Lag= 8.7 min Discarded = 0.16 cfs @ 10.78 hrs, Volume= 0.154 af Primary = 1.24 cfs @ 12.23 hrs, Volume= 0.073 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.31' @ 12.23 hrs Surf.Area= 2,840 sf Storage= 2,280 cf

Plug-Flow detention time= 37.8 min calculated for 0.227 af (100% of inflow) Center-of-Mass det. time= 37.8 min (794.3 - 756.4)

Volume	Invert	Avail.Storage	Storage Description
#1A	136.00'	2,002 cf	34.83'W x 81.52'L x 2.33'H Field A
			6,626 cf Overall - 1,622 cf Embedded = 5,004 cf x 40.0% Voids
#2A	136.50'	1,622 cf	ADS_StormTech SC-310 +Cap x 110 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			110 Chambers in 10 Rows
		3,623 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	136.50'	12.0" Round Culvert
	-		L= 11.5' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 136.50' / 136.05' S= 0.0391 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	136.70'	14.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.83'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	136.00'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.16 cfs @ 10.78 hrs HW=136.02' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.16 cfs)

Primary OutFlow Max=1.24 cfs @ 12.23 hrs HW=137.31' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 1.24 cfs of 1.66 cfs potential flow) -2=Orifice/Grate (Orifice Controls 1.24 cfs @ 3.19 fps)

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Summary for Pond #4: SWM #4

Inflow Area = 0.568 ac, 89.96% Impervious, Inflow Depth = 5.99" for 25-YR event 3.58 cfs @ 12.08 hrs, Volume= Inflow = 0.284 af Outflow = 3.56 cfs @ 12.09 hrs, Volume= 0.284 af, Atten= 0%, Lag= 0.4 min Discarded = 0.04 cfs @ 6.23 hrs, Volume= 0.086 af Primary = 3.53 cfs @ 12.09 hrs, Volume= 0.198 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.75' @ 12.09 hrs Surf.Area= 666 sf Storage= 1,308 cf

Plug-Flow detention time= 90.3 min calculated for 0.284 af (100% of inflow) Center-of-Mass det. time= 90.3 min (848.1 - 757.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	639 cf	11.00'W x 60.58'L x 3.50'H Field A
			2,332 cf Overall - 735 cf Embedded = 1,597 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 2 Rows
		1.374 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
			L= 74.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0135 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.75'	20.0" W x 3.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 6.23 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=3.53 cfs @ 12.09 hrs HW=137.75' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 3.53 cfs of 6.81 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.88 cfs @ 4.51 fps) **3=Sharp-Crested Rectangular Weir** (Weir Controls 1.65 cfs @ 1.65 fps)

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Summary for Link DP1: Spring Brook

Inflow Are	a =	1.907 ac, 8	7.73% Impervio	us, Inflow De	pth = 3.86"	for 25-YR event
Inflow	=	9.72 cfs @	12.10 hrs, Volu	ume=	0.614 af	
Primary	=	9.72 cfs @	12.10 hrs, Volu	ume=	0.614 af, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

REV0 - W211263-PR			Type I	W211263 II 24-hr 1	B Proposed H 00-YR Rain	lydroCAD fall=9.03″
Prepared by Bohler Eng	ineers 3478 © 2022 Hydro	CAD Software Sol	utions LLC		Printed 8	3/30/2023
<u></u>	0470 @ 2022 Hydro					<u>1 age 54</u>
Reach routir	Time span=0.00-7 Runoff by SCS TR- ad by Dyn-Stor-Ind	72.00 hrs, dt=0.0 20 method, UH= method - Pond	1 hrs, 7201 p SCS, Weigh	ooints ted-CN vp-Stor-In	d method	
Reachirodai				yn-0101-m	linethod	
SubcatchmentP1: South	i Edge - Overland F	Runoff Area=0.08 Now Length=394	88 ac 42.05% Tc=6.0 min	6 Imperviou CN=84 R	us Runoff De unoff=0.70 cfs	oth=7.09" 0.052 af
SubcatchmentP2: South	Central	Runoff Area=0.14	40 ac 95.00% Tc=6.0 min	6 Imperviou CN=97 R	us Runoff De unoff=1.24 cfs	pth=8.67" 0.101 af
SubcatchmentP3: East		Runoff Area=0.40	65 ac 87.74% Tc=6.0 min	6 Imperviou CN=95 R	us Runoff De unoff=4.08 cfs	pth=8.43" 0.327 af
SubcatchmentP4: North		Runoff Area=0.44	49 ac 92.65% Tc=6.0 min	6 Imperviou CN=96 R	us Runoff De unoff=3.96 cfs	pth=8.55" 0.320 af
SubcatchmentP5: North	east	Runoff Area=0.1	97 ac 85.28% Tc=6.0 min	6 Imperviou CN=94 R	us Runoff De unoff=1.72 cfs	pth=8.31" 0.136 af
SubcatchmentP6a: Nort	hwest	Runoff Area=0.30	62 ac 84.25% Tc=6.0 min	6 Imperviou CN=94 R	us Runoff De unoff=3.16 cfs	pth=8.31" 0.251 af
SubcatchmentP6b: Nort	hwest (Roof)	Runoff Area=0.200	6 ac 100.00% Tc=6.0 min	6 Imperviou CN=98 R	us Runoff De unoff=1.83 cfs	pth=8.79" 0.151 af
Reach R1: Spring Brook				In Out	flow=12.18 cfs flow=12.18 cfs	0.824 af 0.824 af
Reach R2: East Street				l Ou	nflow=1.94 cfs itflow=1.94 cfs	0.143 af 0.143 af
Pond #1: SWM #1		Peak Elev=13	37.71' Storage	e=467 cf li Ou	nflow=1.24 cfs Itflow=1.24 cfs	0.101 af 6 0.091 af
Pond #2: SWM #2	Discarded=0.04 cfs	Peak Elev=137. 0.084 af Primar	.72' Storage= y=4.03 cfs 0.2	1,287 cf li 242 af Ou	nflow=4.08 cfs tflow=4.07 cfs	0.327 af 0.327 af
Pond #3: SWM #3	Discarded=0.16 cfs	Peak Elev=137. 0.186 af Primar	.86' Storage= y=1.94 cfs 0.	3,089 cf li 134 af Ou	nflow=3.96 cfs tflow=2.10 cfs	0.320 af 0.320 af
Pond #4: SWM #4	Discarded=0.04 cfs	Peak Elev=137. 0.090 af Primar	.87' Storage= y=4.94 cfs 0.3	1,340 cf li 312 af Ou	nflow=4.99 cfs tflow=4.98 cfs	0.401 af 0.401 af
Link DP1: Spring Brook				In Prin	flow=14.12 cfs nary=14.12 cfs	0.967 af 0.967 af
Total Rui	noff Area = 1.907 a	ac Runoff Volu 12.27% Pervious	me = 1.337 a s = 0.234 ac	af Avera 87.73%	ge Runoff De Impervious	epth = 8.42" = 1.673 ac

Summary for Subcatchment P1: South Edge - Overland

Runoff	=	0.70 cfs @	12.08 hrs,	Volume=	0.052 af,	Depth=	7.09"
Routed	to R	each R2 : East S	Street				

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area	(ac) (CN D	escription		
0.	051	74 >7	′5% Grass c	over, Good,	, HSG C
0.	037	98 Pa	aved parking	, HSG C	
0.	088	84 W	eighted Ave	rage	
0.	051	57	.95% Pervic	us Area	
0.	037	42	2.05% Imper	vious Area	
Tc (min)	Length (feet)	Slop (ft/f	e Velocity t) (ft/sec)	Capacity (cfs)	Description
0.6	50	0.026	0 1.38		Sheet Flow, 143.3-142
2.6	344	0.012	2.22		Smooth surfaces n= 0.011 P2= 3.46" Shallow Concentrated Flow, 142-137.74 Paved Kv= 20.3 fps
3.2	394	Total	Increased	to minimum	Tc = 6.0 min

Summary for Subcatchment P2: South Central

Runoff	=	1.24 cfs @	12.08 hrs,	Volume=
Routed	to	Pond #1 : SWM #	1	

0.101 af, Depth= 8.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area ((ac)	CN	Desc	ription						
0.1	133	98	Pave	aved parking, HSG C						
0.0	007	74	>75%	6 Grass co	over, Good	, HSG C				
0.1	140	97	Weig	hted Aver	age					
0.0	007		5.00	% Perviou	s Area					
0.1	133		95.00	0% Imperv	vious Area					
Тс	Lena	th S	Slope	Velocitv	Capacity	Description				
(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)					
6.0						Direct Entry.				

Direct Entry,

Summary for Subcatchment P3: East

4.08 cfs @ 12.08 hrs, Volume= Runoff = Routed to Pond #2 : SWM #2

0.327 af, Depth= 8.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

W211263 Proposed HydroCAD *Type III 24-hr 100-YR Rainfall=9.03"* Printed 8/30/2023 Iutions LLC Page 36

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Area	(ac)	CN	Desc	ription							
0.	211	98	Pave	ved parking, HSG C							
0.	197	98	Roof	pofs, HSG C							
0.	057	74	>75%	6 Grass co	over, Good	, HSG C					
0.	465	95	Weig	hted Aver	age						
0.	057		12.2	5% Pervio	us Area						
0.	408		87.74	4% Imper	vious Area						
Tc (min)	Leng (fee	th t)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
6.0						Direct Entry,					

Summary for Subcatchment P4: North

Runoff = 3.96 cfs @ 12.08 hrs, Volume= Routed to Pond #3 : SWM #3 0.320 af, Depth= 8.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area (ac	;) CN	Desc	cription		
0.25	3 98	B Pave	ed parking	, HSG C	
0.16	3 98	Roof	s, HSG C		
0.03	3 74	>75%	% Grass co	over, Good	d, HSG C
0.44	9 96	i Weig	ghted Aver	age	
0.03	3	7.35	% Perviou	s Area	
0.41	6	92.6	5% Imper	ious Area/	
To Le	enath	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0					Direct Entry,

Summary for Subcatchment P5: Northeast

Runoff = 1.72 cfs @ 12.08 hrs, Volume= 0.136 af, Depth= 8.31" Routed to Reach R1 : Spring Brook

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area (ac)	CN	Description
0.168	98	Paved parking, HSG C
0.029	74	>75% Grass cover, Good, HSG C
0.197	94	Weighted Average
0.029		14.72% Pervious Area
0.168		85.28% Impervious Area

REV0 ·	- W2112	263-PR			Type III 24-hr 100-YR Rainfall=9.03				
Prepare	d by Bo	hler Engi	neers		Printed 8/30/2023				
HydroCA	<u>D® 10.20</u>	-2g_s/n 03	3478 © 202	22 HydroCA	D Software Solutions LLC Page 37				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
6.0					Direct Entry,				
			Summar	ry for Sub	bcatchment P6a: Northwest				
Runoff Rout	= ed to Por	3.16 cf nd #4 : SV	s @ 12.0 VM #4	8 hrs, Volu	ume= 0.251 af, Depth= 8.31"				
Runoff b Type III	oy SCS T 24-hr 10	R-20 met 0-YR Rai	hod, UH=S nfall=9.03'	SCS, Weigh '	hted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs				
Area	(ac) C	N Des	cription						
0 0	.305 9 .057 7	98 Pave 74 >75	ed parking % Grass c	, HSG C over, Good	I, HSG C				
0 0 0	.362 9 .057 .305	94 Weig 15.7 84.2	ghted Aver 5% Pervic 5% Imper	rage ous Area vious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				

Summary for Subcatchment P6b: Northwest (Roof)

Direct Entry,

Runoff = 1.83 cfs @ 12.08 hrs, Volume= Routed to Pond #4 : SWM #4

6.0

0.151 af, Depth= 8.79"

W211263 Proposed HydroCAD

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Type III 24-hr 100-YR Rainfall=9.03"

Area (a	ic) (CN De	scri	ption		
0.2	06	98 Ro	ofs,	HSG C		
0.20	06	10	0.00)% Impe	rvious Area	a
Tc l (min)	_ength (feet)	Slop (ft/f	e ∖ :)	/elocity (ft/sec)	Capacity (cfs)	Description
6.0				•		Direct Entry,

Summary for Reach R1: Spring Brook

Inflow Area = 1.679 ac, 89.52% Impervious, Inflow Depth = 5.89" for 100-YR event Inflow = 12.18 cfs @ 12.09 hrs, Volume= 0.824 af Outflow = 12.18 cfs @ 12.09 hrs, Volume= 0.824 af, Atten= 0%, Lag= 0.0 min Routed to Link DP1 : Spring Brook Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Reach R2: East Street

Inflow Area = 0.228 ac, 74.56% Impervious, Inflow Depth = 7.53" for 100-YR event Inflow = 1.94 cfs @ 12.09 hrs, Volume= 0.143 af Outflow = 1.94 cfs @ 12.09 hrs, Volume= 0.143 af, Atten= 0%, Lag= 0.0 min Routed to Link DP1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

Summary for Pond #1: SWM #1

Inflow Area	ı =	0.140 ac, 9	5.00% Impe	ervious, Inflow	/ Depth = 8	8.67" for	100-YR event
Inflow	=	1.24 cfs @	12.08 hrs,	Volume=	0.101 a	af	
Outflow	=	1.24 cfs @	12.09 hrs,	Volume=	0.091 a	af, Atten= (0%, Lag= 0.3 min
Primary	=	1.24 cfs @	12.09 hrs,	Volume=	0.091 a	af	•
Routed	to Reac	h R2 : East S	Street				

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.71' @ 12.09 hrs Surf.Area= 281 sf Storage= 467 cf

Plug-Flow detention time= 93.0 min calculated for 0.091 af (90% of inflow) Center-of-Mass det. time= 43.3 min (788.5 - 745.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	283 cf	15.75'W x 17.86'L x 3.50'H Field A
			984 cf Overall - 276 cf Embedded = 709 cf x 40.0% Voids
#2A	135.50'	276 cf	ADS_StormTech SC-740 +Cap x 6 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			6 Chambers in 3 Rows
		559 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.70'	12.0" Round Culvert L= 17.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.50' / 135.70' S= -0.0118 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	137.50'	4.0' Iong Sharp-Crested Rectangular Weir 2 End Contraction(s)

Primary OutFlow Max=1.24 cfs @ 12.09 hrs HW=137.71' TW=0.00' (Dynamic Tailwater)

1-2=Sharp-Crested Rectangular Weir (Weir Controls 1.24 cfs @ 1.49 fps)

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Summary for Pond #2: SWM #2

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Inflow Area = 0.465 ac, 87.74% Impervious, Inflow Depth = 8.43" for 100-YR event 4.08 cfs @ 12.08 hrs, Volume= Inflow = 0.327 af Outflow = 4.07 cfs @ 12.09 hrs, Volume= 0.327 af, Atten= 0%, Lag= 0.4 min Discarded = 0.04 cfs @ 5.18 hrs, Volume= 0.084 af Primary = 4.03 cfs @ 12.09 hrs, Volume= 0.242 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.72' @ 12.09 hrs Surf.Area= 658 sf Storage= 1,287 cf

Plug-Flow detention time= 71.9 min calculated for 0.327 af (100% of inflow) Center-of-Mass det. time= 71.9 min (826.5 - 754.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	627 cf	20.50'W x 32.10'L x 3.50'H Field A
			2,303 cf Overall - 735 cf Embedded = 1,568 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 4 Rows
		1,362 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	-		L= 183.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.50'	20.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 5.18 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=4.03 cfs @ 12.09 hrs HW=137.72' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 4.03 cfs of 6.23 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 2.74 cfs @ 4.93 fps)

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Summary for Pond #3: SWM #3

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Inflow Area = 0.449 ac, 92.65% Impervious, Inflow Depth = 8.55" for 100-YR event 3.96 cfs @ 12.08 hrs, Volume= Inflow = 0.320 af Outflow = 2.10 cfs @ 12.21 hrs, Volume= 0.320 af, Atten= 47%, Lag= 7.6 min Discarded = 0.16 cfs @ 9.82 hrs, Volume= 0.186 af Primary = 1.94 cfs @ 12.21 hrs, Volume= 0.134 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.86' @ 12.21 hrs Surf.Area= 2,840 sf Storage= 3,089 cf

Plug-Flow detention time= 37.4 min calculated for 0.320 af (100% of inflow) Center-of-Mass det. time= 37.4 min (787.6 - 750.1)

Volume	Invert	Avail.Storage	Storage Description
#1A	136.00'	2,002 cf	34.83'W x 81.52'L x 2.33'H Field A
			6,626 cf Overall - 1,622 cf Embedded = 5,004 cf x 40.0% Voids
#2A	136.50'	1,622 cf	ADS_StormTech SC-310 +Cap x 110 Inside #1
			Effective Size= 28.9"W x 16.0"H => 2.07 sf x 7.12'L = 14.7 cf
			Overall Size= 34.0"W x 16.0"H x 7.56'L with 0.44' Overlap
			110 Chambers in 10 Rows
		3,623 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	136.50'	12.0" Round Culvert
	-		L= 11.5' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 136.50' / 136.05' S= 0.0391 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	136.70'	14.0" W x 4.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.83'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	136.00'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.16 cfs @ 9.82 hrs HW=136.02' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.16 cfs)

Primary OutFlow Max=1.94 cfs @ 12.21 hrs HW=137.86' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 1.94 cfs of 2.77 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.87 cfs @ 4.80 fps)

3=Sharp-Crested Rectangular Weir (Weir Controls 0.08 cfs @ 0.59 fps)

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Summary for Pond #4: SWM #4

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Inflow Area = 0.568 ac, 89.96% Impervious, Inflow Depth = 8.48" for 100-YR event 4.99 cfs @ 12.08 hrs, Volume= Inflow = 0.401 af Outflow = 4.98 cfs @ 12.09 hrs, Volume= 0.401 af, Atten= 0%, Lag= 0.4 min Discarded = 0.04 cfs @ 4.23 hrs, Volume= 0.090 af Primary = 4.94 cfs @ 12.09 hrs, Volume= 0.312 af Routed to Reach R1 : Spring Brook

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs Peak Elev= 137.87' @ 12.09 hrs Surf.Area= 666 sf Storage= 1,340 cf

Plug-Flow detention time= 69.8 min calculated for 0.401 af (100% of inflow) Center-of-Mass det. time= 69.8 min (821.4 - 751.5)

Volume	Invert	Avail.Storage	Storage Description
#1A	134.50'	639 cf	11.00'W x 60.58'L x 3.50'H Field A
			2,332 cf Overall - 735 cf Embedded = 1,597 cf x 40.0% Voids
#2A	135.00'	735 cf	ADS_StormTech SC-740 +Cap x 16 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			16 Chambers in 2 Rows
		1.374 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	135.00'	15.0" Round Culvert
	•		L= 74.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 135.00' / 134.00' S= 0.0135 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf
#2	Device 1	136.75'	20.0" W x 3.0" H Vert. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#3	Device 1	137.50'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	134.50'	2.410 in/hr Exfiltration over Surface area Phase-In= 0.01'

Discarded OutFlow Max=0.04 cfs @ 4.23 hrs HW=134.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.04 cfs)

Primary OutFlow Max=4.94 cfs @ 12.09 hrs HW=137.87' TW=0.00' (Dynamic Tailwater) -1=Culvert (Passes 4.94 cfs of 7.00 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 2.00 cfs @ 4.81 fps)

Summary for Link DP1: Spring Brook

 Inflow Area =
 1.907 ac, 87.73% Impervious, Inflow Depth =
 6.09" for 100-YR event

 Inflow =
 14.12 cfs @
 12.09 hrs, Volume=
 0.967 af

 Primary =
 14.12 cfs @
 12.09 hrs, Volume=
 0.967 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.01 hrs

APPENDIX F: STORMWATER CALCULATIONS

- > MA STANDARD #3 RECHARGE AND DRAWDOWN TIME
- MA STANDARD #4 WATER QUALITY AND TSS REMOVAL
- > <u>STAGE STORAGE VOLUME</u>
- WATER QUALITY UNIT SIZING
- ➢ <u>PIPE SIZING</u>
- ➢ RAINFALL DATA
- RAINFALL INTENSITY DATA

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA Bohler Job Number: W211263 August 30, 2023

MA DEP Standard 3: Recharge Volume Calculations

Required Recharge Volume - A Soils (0.60 in.)			
Existing Site Impervious Area (ac)	0.000		
Proposed Site Impervious Area (ac)	0.000		
Proposed Increase in Site Impervious Area (ac)	0.000		
Recharge Volume Required (cf)	0		

Required Recharge Volume - B Soils (0.35 in.)			
Existing Site Impervious Area (ac)	0.000		
Proposed Site Impervious Area (ac)	0.000		
Proposed Increase in Site Impervious Area (ac)	0.000		
Recharge Volume Required (cf)	0		

Required Recharge Volume - C Soils (0.25 in.)			
Existing Site Impervious Area (ac)	1.561		
Proposed Site Impervious Area (ac)	1.673		
Proposed Increase in Site Impervious Area (ac)	0.112		
Recharge Volume Required (cf)	102		

Required Recharge Volume - D Soils (0.10 in.)			
Existing Site Impervious Area (ac)	0.000		
Proposed Site Impervious Area (ac)	0.000		
Proposed Increase in Site Impervious Area (ac)	0.000		
Recharge Volume Required (cf)	0		

|--|

Recharge Volume Adjustment Factor	
Impervious Area Directed to Infiltration BMP (ac)	1.454
%Impervious Directed to Infiltration BMP	87%
Adjustment Factor	1.15
Adjusted Total Recharge Volume Required (cf)	117

Provided Recharge Volume*	
SWM #1	436
SWM #2	865
SWM #3	1,018
SWM #4	979
Total Recharge Volume Provided (cf)	3,298
	Provided greater than or Equal to Required

*Volume provided below lowest outlet in cubic feet (cf)



Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA Bohler Job Number: W211263 August 30, 2023

MA DEP Standard 3: Drawdown Time Calculations

Drawdown Time - SWM #1	
Volume below outlet pipe (Rv) (cf)	436
Soil Type	Sandy Loam - B
Infiltration rate (K)*	1.02
Bottom Area (sf)	281
Drawdown time (Hours)*	18.3
Drawdown Time - SWM #2	
Volume below outlet pipe (Rv) (cf)	865
Soil Type	Loamy Sand - A
Infiltration rate (K)*	2.41
Bottom Area (sf)	658
Drawdown time (Hours)**	6.5
Drawdown Time - SWM #3	
Volume below outlet pipe (Rv) (cf)	1,018
Soil Type	Loamy Sand - A
Infiltration rate (K)*	2.41
Bottom Area (sf)	2,839
Drawdown time (Hours)**	1.8
Drawdown Time - SWM #4	
Volume below outlet pipe (Rv) (cf)	979
Soil Type	Loamy Sand - A
Infiltration rate (K)*	2.41
Bottom Area (sf)	666
Drawdown time (Hours)**	7.3

*Infiltration Rates taken from Rawls Table

**Drawdown time = Rv / (K) x (bottom area)


MA DEP Standard 4: Water Quality Volume Calculations

Water Quality Volume Required	
Water Quality Volume runoff (in.)*	0.5
Total Post Development Impervious Area (sf)	72,876
Required Water Quality Volume (cf)	3,036
*Water Quality volume runoff is equal to 0.5 inches of runoff	times the total impervious area of the post
development project site (including roof)	

Water Quality Volume Provided*	
SWM #1	436
SWM #2	865
SWM #3	1,018
SWM #4	979
Total Provided Water Quality Volume (cf)	3,298
	Required Recharge Provided

*Volume provided below lowest outlet pipe in cubic feet (cf)



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Pretreatment to SWM#1 (CB to Isolator Row)

A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining
BMP	Rate	Load*	Removed (B*C)	Load (C-D)
Deep Sump Hooded Catch Basin	0.25	1.00	0.25	0.75
Isolator Row	0.25	0.75	0.19	0.56
	<u>.</u>	Total TSS Removal =	44%	



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Treatment at SWM#1 (Underground Infiltration System)

	-	-		
A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining
BMP	Rate	Load*	Removed (B*C)	Load (C-D)
Deep Sump Hooded Catch	0.25	1.00	0.25	0.75
Basin	0.25	1.00	0.25	0:75
Underground Infiltration				
System (Stormtech SC-740)	0.80	0.75	0.60	0.15
with isolator row	0.00	0.75	0.00	0.15
pretreatment				
			05%/	
		i otal 155 Removal =	85%	J



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Pretreatment to SWM#2-4 (CB to Isolator Row)

A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining
BMP	Rate	Load*	Removed (B*C)	Load (C-D)
Deep Sump Hooded Catch Basin	0.25	1.00	0.25	0.75
Isolator Row	0.25	0.75	0.19	0.56
		Total TSS Removal =	44%	



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Treatment at SWM#2 & 4 (Underground Infiltration System)

	-	-		
A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining
BMP	Rate	Load*	Removed (B*C)	Load (C-D)
Deep Sump Hooded Catch	0.25	1.00	0.25	0.75
Basin				
System (Stormtech SC-740)				
with isolator row	0.80	0.75	0.60	0.15
pretreatment				
		Total TSS Removal =	85%	
				4



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Treatment at SWM#3 (Underground Infiltration System)

A	В	С	D	E
	TSS Removal	Starting TSS	Amount	Remaining
BMP	Rate	Load*	Removed (B*C)	Load (C-D)
Deep Sump Hooded Catch	0.25	1.00	0.25	0.75
Basin	0.25	1.00	0.25	0:75
Underground Infiltration				
System (Stormtech SC-310)	0.80	0.75	0.60	0.15
with isolator row	0.00	0.75	0.00	0.15
pretreatment				
			05%/	
		i otal 155 Removal =	85%	J



MA DEP Standard 4: TSS Removal Calculation Worksheet

BMP Treatment Train: Treatment at Proprietary Water Quality Inlet (WQi500)

A BMP	B TSS Removal Rate	C Starting TSS Load*	D Amount Removed (B*C)	E Remaining Load (C-D)
Proprietary Water Quality Inlet (WQi500)	0.80	1.00	0.80	0.20
		Total TSS Removal =	80%	



MA DEP Standard 4: Weighted TSS Removal Rate

Design Point - Treatment Train Description(s)	TSS Removal (%)	Treated Imp. Area* (ac)	TSS Removal (%)	Untreated Imp. Area (ac)	Total Area
DP1 - Overland to East Street	0.00	0.000	0.00	0.037	0.037
DP1 - To Wqi500	0.80	0.168	0.12	0.000	0.168
DP1 - CBs to UG Basins 1-4 w/ pretreatment	0.85	0.902	0.69	0.000	0.902
Total Weighted TSS Removal Rate	0.81				1.107

*Excludes roof runoff

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8/29/2023

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Stage-Area-Storage for Pond #1: SWM #1 (continued)

Elevation	Storage	Elevation	Storage	Elevation	Storage
	(cubic-reet)		(cubic-feet)		(cubic-reet)
136.53	264	137.04	359	137.55	444
136.54	266	137.05	361	137.56	446
136.55	268	137.06	363	137.57	447
136.56	270	137.07	364	137.58	449
136.57	272	137.08	366	137.59	450
136.58	274	137.09	368	137.60	452
136.59	276	137.10	370	137.61	453
136.60	278	137.11	371	137.62	455
136.61	280	137.12	373	137.63	456
136.62	281	137.13	375	137.64	457
136.63	283	137.14	377	137.65	459
136.64	285	137.15	378	137.66	460
136.65	287	137.16	380	137.67	462
136.66	289	137.17	382	137.68	463
136.67	291	137.18	384	137.69	465
136.68	293	137.19	385	137.70	466
136.69	295	137.20	387	137.71	467
136.70	297	137.21	389	137.72	469
136.71	298	137.22	390	137.73	470
136.72	300	137.23	392	137.74	471
136.73	302	137.24	394	137.75	473
136.74	304	137.25	396	137.76	474
136.75	306	137.26	397	137.77	475
136.76	308	137.27	399	137.78	477
136.77	310	137.28	401	137.79	478
136.78	312	137.29	402	137.80	479
136.79	313	137.30	404	137.81	480
136.80	315	137.31	406	137.82	482
136.81	317	137.32	407	137.83	483
136.82	319	137.33	409	137.84	484
136.83	321	137.34	411	137.85	485
136.84	323	137.35	412	137.86	487
136.85	325	137.36	414	137.87	488
136.86	326	137.37	415	137.88	489
136.87	328	137.38	417	137.89	490
136.88	330	137.39	419	137.90	491
136.89	332	137.40	420	137.91	493
136.90	334	137.41	422	137.92	494
136 91	336	137 42	424	137.93	495
136.92	337	137 43	425	137.94	496
136.93	339	137 44	427	137.95	497
136.94	341	137 45	428	137.96	498
136.95	343	137.46	430	137.97	499
136.96	345	137 47	432	137.98	501
136.97	346	137.48	433	137.99	502
136.98	348	137 49	435	138.00	502
136.99	350	137 50	436	138.01	504
137.00	352	137 51	438	138.02	505
137.00	354	137 52	430	138.02	505
137.02	355	137 53	400	138.04	507
137.02	357	137 54	442	138.05	508
101.00	007		774		000

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Stage-Area-Storage for Pond #2: SWM #2 (continued)

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
135.52	658	398	136.03	658	648
135.53	658	403	136.04	658	653
135.54	658	408	136.05	658	658
135.55	658	413	136.06	658	662
135.56	658	418	136.07	658	667
135.57	658	423	136.08	658	672
135.58	658	428	136.09	658	677
135.59	658	433	136.10	658	681
135.60	658	438	136.11	658	686
135.61	658	443	136.12	658	691
135.62	658	448	136.13	658	696
135.63	658	453	136.14	658	700
135.64	658	458	136.15	658	705
135.65	658	463	136.16	658	/10
135.66	658	468	136.17	658	714
135.67	658	473	136.18	658	719
135.68	658	478	136.19	658	724
135.69	658	483	136.20	658	728
135.70	658	488	136.21	658	/ 33
135.71	658	493	136.22	658	738
135.72	658	497	130.23	658	742
135.73	000	50Z	130.24	000	747
135.74	658	507	130.25	658	752
135.75	000	51Z 517	130.20	000	700
133.70	000	517	130.27	000	701
133.77	000	52Z 527	130.20	000	700
135.70	000	527	130.29	000	770
135.79	000	53Z	130.30	000	770
135.00	658	537	130.31	658	79/
135.01	000	54Z	130.32	000	704
135.02	658	552	136.34	658	700
135.84	658	556	136.35	658	793
135.85	658	561	136.36	658	802
135.86	658	566	136.37	658	806
135.87	658	571	136.38	658	811
135.88	658	576	136.39	658	815
135.89	658	581	136 40	658	820
135.90	658	586	136 41	658	824
135.91	658	590	136 42	658	829
135.92	658	595	136 43	658	833
135.93	658	600	136 44	658	838
135.94	658	605	136 45	658	842
135.95	658	610	136 46	658	847
135.96	658	615	136.47	658	851
135.97	658	619	136.48	658	856
135.98	658	624	136.49	658	860
135.99	658	629	136.50	658	865
136.00	658	634	136.51	658	869
136.01	658	639	136.52	658	873
136.02	658	643	136.53	658	878

REV0 - W211263-PR

Stage Storage Tables *Type III 24-hr 2-YR Rainfall=3.46"* Printed 8/29/2023 <u>C Page 8</u>

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Stage-Area-Storage for Pond #3: SWM #3

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
136.00	2,840	0	136.51	2,840	591
136.01	2,840	11	136.52	2,840	613
136.02	2,840	23	136.53	2,840	636
136.03	2,840	34	136.54	2,840	659
136.04	2,840	45	136.55	2,840	681
136.05	2,840	57	136.56	2,840	704
136.06	2,840	68	136.57	2,840	726
136.07	2,840	80	136.58	2,840	749
136.08	2,840	91	136.59	2,840	772
136.09	2.840	102	136.60	2.840	794
136.10	2,840	114	136.61	2.840	817
136.11	2,840	125	136.62	2.840	839
136.12	2.840	136	136.63	2.840	862
136.13	2,840	148	136.64	2.840	884
136.14	2,840	159	136.65	2.840	906
136 15	2 840	170	136.66	2 840	929
136 16	2 840	182	136 67	2 840	951
136 17	2 840	193	136.68	2 840	973
136.18	2 840	204	136 69	2 840	996
136 19	2,810	216	136 70	2,840	1 018
136.20	2 840	227	136 71	2 840	1,040
136.21	2,840	239	136 72	2,840	1,010
136.22	2,040	250	136 73	2,040	1,002
136.23	2,040	261	136 74	2,040	1,004
136.24	2,040	273	136 75	2,040	1 128
136.25	2,040	284	136 76	2,040	1,120
136.26	2,040	204	136.70	2,040	1,100
136.27	2,040	307	136 78	2,040	1 104
136.28	2,040	318	136 79	2,040	1,104
136.20	2,040	320	136.80	2,040	1,210
136.20	2,040	3/1	136.81	2,040	1,250
136 31	2,040	352	136.82	2,040	1,200
136.32	2,040	363	136.83	2,040	1,201
136.32	2,040	375	136.84	2,040	1,303
136.34	2,040	386	136.85	2,040	1,325
136.35	2,040	308	136.86	2,040	1,340
136.36	2,040	400	136.87	2,040	1 380
136.37	2,040	409	136.88	2,040	1,309
136.39	2,040	420	136.00	2,040	1,411
130.30	2,040	432	130.09	2,040	1,452
136.40	2,040	443	136.01	2,040	1,434
130.40	2,040	404	136.02	2,040	1,475
130.41	2,040	400	130.92	2,040	1,490
130.42	2,040	477	130.93	2,040	1,517
130.43	2,040	400	130.94	2,040	1,000
130.44	2,040	500	130.95	2,040	1,559
130.43	2,040	511	130.90	2,040	1,000
130.40	2,040	522	130.97	2,040	1,001
100.47	2,040	004 EAE	130.90	2,040	1,022
100.40	2,040	040 EE7	100.99	2,040	1,043
130.49	2,040	00 <i>1</i>	137.00	2,040	1,004
130.30	∠,040	500	137.01	2,040	1,000

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Stage-Area-Storage for Pond #4: SWM #4 (continued)

Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
136.54	666	889	137.05	666	1,099
136.55	666	893	137.06	666	1,102
136.56	666	898	137.07	666	1,106
136.57	666	902	137.08	666	1,110
136.58	666	907	137.09	666	1,114
136.59	666	911	137.10	666	1,117
136.60	666	915	137.11	666	1,121
136.61	666	920	137.12	666	1,124
136.62	666	924	137.13	666	1,128
136.63	666	928	137.14	666	1,132
136.64	666	933	137.15	666	1,135
136.65	666	937	137.16	666	1,139
136.66	666	941	137.17	666	1,142
136.67	666	946	137.18	666	1,146
136.68	666	950	137.19	666	1,149
136.69	666	954	137.20	666	1,152
136.70	666	958	137.21	666	1,156
136.71	666	963	137.22	666	1,159
136.72	666	967	137.23	666	1,162
136.73	666	971	137.24	666	1,165
136.74	666	975	137.25	666	1,169
136.75	666	979	137.26	666	1,172
136.76	666	984	137.27	666	1,175
136.77	666	988	137.28	666	1,178
136.78	666	992	137.29	666	1,181
136.79	666	996	137.30	666	1,184
136.80	666	1,000	137.31	666	1,187
136.81	666	1,004	137.32	666	1,190
136.82	666	1,008	137.33	666	1,193
136.83	666	1,012	137.34	666	1,196
136.84	666	1,016	137.35	666	1,199
136.85	666	1,021	137.36	666	1,202
136.86	666	1,025	137.37	666	1,205
136.87	666	1,029	137.38	666	1,208
136.88	666	1,033	137.39	666	1,210
136.89	666	1,037	137.40	666	1,213
136.90	666	1,041	137.41	666	1,216
136.91	666	1,045	137.42	666	1,219
136.92	666	1,049	137.43	666	1,222
136.93	666	1,053	137.44	666	1,224
136.94	666	1,056	137.45	666	1,227
136.95	666	1,060	137.46	666	1,230
136.96	666	1,064	137.47	666	1,233
136.97	666	1,068	137.48	666	1,235
136.98	666	1,072	137.49	666	1,238
136.99	666	1,076	137.50	666	1,241
137.00	666	1,080	137.51	666	1,243
137.01	666	1,084	137.52	666	1,246
137.02	666	1,087	137.53	666	1,249
137.03	666	1,091	137.54	666	1,251
137.04	666	1,095	137.55	666	1,254

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA Bohler Job Number: W211263 8/30/2023 1" Water Quality Volume to Flow Rate Calculation Sheet

Compute Water Quality Flow with the following Equation

WQF = (qu)(A)(WQV)

Site Plan Callout		qu (from 1" - qu Table)	Impervious Area (SF)	Ai (sq/mi)	WQV (inches)		WQF (cfs)
Wqi500	=	774	7318	0.000262	1	=	0.20
Water Quality Flow I Water Quality Volun	Rate = ne =	= /in) -	WQF WQV*				

Unit peak discharge (csm/in) = qu Impervious Area in watershed (square miles) = Ai

*WQV is expressed in watershed inches (you must use 1.0-inches in all cases with this method and not 0.5-inches)

** calculate the qu based on the time of concentration (see 1" - qu Table)



<u>1" qu Sheet</u>

	Tc (hours)	qu (csm/in)	
	0.01	835	
	0.03	835	
	0.05	831	
	0.067	814	
5 Minutes	0.083	795	
	0.1	774	<
	0.116	755	
	0.133	736	
	0.15	717	
10 minutes	0.167	700	
	0.183	685	
	0.2	669	
	0.217	654	
	0.233	641	
15 minutes	0.25	628	
	0.3	593	
	0.333	572	
	0.35	563	
	0.4	536	
	0.416	528	
	0.5	491	
	0.583	460	
	0.6	454	
	0.667	433	
	0.7	424	
	0.8	398	
	0.9	376	
	1	356	
	1.1	339	
	1.2	323	
	1.3	309	
	1.4	296	
	1.5	285	
	1.6	274	
	1.7	264	
	1.8	255	
	1.9	247	
	2	239	
	2.1	232	
	2.2	225	
	2.3	219	
	2.4	213	
	2.5	207	
	2.6	202	

Tc (hours)	qu (csm/in)
2.7	197
2.8	192
2.9	187
3	183
3.1	179
3.2	175
3.3	171
3.4	168
3.5	164
3.6	161
3.7	158
3.8	155
3.9	152
4	149
4.1	146
4.2	144
4.3	141
4.4	139
4.5	137
4.6	134
4.7	132
4.8	130
4.9	128
5	126
5.1	124
5.2	122
5.3	120
5.4	119
5.5	117
5.6	115
5.7	114
5.8	112
5.9	111
6	109
6.1	108
6.2	106
6.3	105
6.4	104
6.5	102
6.6	101
6.7	100
6.8	99
6.9	98
7	96

Tc (hours)	qu (csm/in)
7.1	95
7.2	94
7.3	93
7.4	92
7.5	91
7.6	90
7.7	89
7.8	88
7.9	87
8	86
8.1	85
8.2	84
8.3	84
8.4	83
8.5	82
8.6	81
8.7	80
8.8	79
8.9	79
9	78
9.1	77
9.2	76
9.3	76
9.4	75
9.5	74
9.6	74
9.7	73
9.8	72
9.9	72
10	71

*Table of qu values for la/P Curve =0.034, listed by Tc, for Type III Storm Distribution http://www.mass.gov/eea/docs/dep/water/resources/07v5/13wqvwqf.pdf

Rational Pipe Sizing Calculations

Design Pe	riod Storm	100	Year	Design	Period Int	ensity*	11.3	in/hr	1							
LOCA	TION	I	IMPERVIO	JS		OTHER	-	SUM	Тс		Q	D	S			Q Full
FROM	то	А	С	CA	А	С	CA	CA	(min)	(in/hr)	(cfs)	(in)	(ft/ft)	Matieral	n	(cfs)
AD01	DMH100	0.01	0.95	0.01	0.01	0.30	0.00	0.01	6	11.3	0.14	12	0.013	HDPE	0.012	4.40
CB100	DMH100	0.03	0.95	0.03	0.00	0.30	0.00	0.03	6	11.3	0.32	12	0.024	HDPE	0.012	5.98
CB101	DMH101	0.09	0.95	0.09	0.01	0.30	0.00	0.09	6	11.3	1.00	12	0.012	HDPE	0.012	4.23
CB200	DMH200	0.09	0.95	0.09	0.03	0.30	0.01	0.09	6	11.3	1.07	12	0.006	HDPE	0.012	2.99
CB201	DMH201	0.11	0.95	0.10	0.03	0.30	0.01	0.11	6	11.3	1.28	12	0.025	HDPE	0.012	6.10
OCS200	DMH202				HydroCAD	25-year ste	orm (UG2)				4.03	15	0.006	HDPE	0.012	5.42
CB400	DMH400	0.16	0.95	0.15	0.05	0.30	0.02	0.17	6	11.3	1.89	12	0.008	HDPE	0.012	3.45
CB401	DMH400	0.11	0.95	0.10	0.01	0.30	0.00	0.11	6	11.3	1.21	12	0.009	HDPE	0.012	3.66
DS3	DMH400	0.21	0.95	0.20	0.00	0.30	0.00	0.20	6	11.3	2.25	12	0.010	HDPE	0.012	3.86
OCS400	DMH202			-	HydroCAD	25-year sto	orm (UG4)	-	-	-	4.94	15	0.012	HDPE	0.012	7.50
DMH202	DMH203			l Hy	droCAD 25	-year storm	l n (UG2+UG	4)			8.97	18	0.010	HDPE	0.012	11.38
CB300	DMH302	0.12	0.95	0.11	0.01	0.30	0.00	0.12	6	11.3	1.32	12	0.010	HDPE	0.012	3.86
DS4	DMH302	0.16	0.95	0.15	0.00	0.30	0.00	0.15	6	11.3	1.72	12	0.008	HDPE	0.012	3.36
DMH302	DMH300	0.28	0.95	0.27	0.01	0.30	0.00	0.27	6	11.3	3.04	12	0.008	HDPE	0.012	3.45
OCS300	DMH203				HvdroCAD	25-vear st	orm (UG3)				1.94	12	0.039	HDPE	0.012	7.62
DMH203	DMH204			Hydro	CAD 25-ye	ar storm (L	JG2+UG3+I	UG4)			10.91	18	0.013	HDPE	0.012	12.97
WQi500	DMH204	0.17	0.95	0.16	0.03	0.30	0.01	0.17	6	11.3	1.93	12	0.010	HDPE	0.012	3.86
DMH204	Out			HydroCAD	25-year sto	orm (UG2+l	UG3+UG4)	+ WQi500			12.84	24	0.012	HDPE	0.012	26.62
1					1			1	1	I						I

*Rainfall intesity provided by NOAA Atlas 14, Volume 10, Version 2 on 8/30/23

Prepared By: BOHLER// 352 Turnpike Road Southborough, MA 01772 (508) 480-9900

V Full (fps)
5.60
7.61
5.38
3.81
7.77
4.42
4.40
4.66
4.91
6.12
6.44
4.91
4.28
4.40
9.70
7.34
4.91
8.47
I

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point											
Smoothing	Yes										
State											
Location											
Latitude	42.147 degrees North										
Longitude	71.254 degrees West										
Elevation	40 feet										
Date/Time	Tue May 09 2023 14:13:45 GMT-0400 (Eastern Daylight Time)										

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.29	0.44	0.55	0.72	0.90	1.14	1yr	0.78	1.07	1.32	1.67	2.12	2.71	2.98	1yr	2.40	2.87	3.34	3.98	4.68	1yr
2yr	0.36	0.55	0.68	0.90	1.13	1.43	2yr	0.98	1.32	1.65	2.07	2.60	3.26	3.62	2yr	2.88	3.48	3.98	4.74	5.37	2yr
5yr	0.43	0.67	0.84	1.13	1.44	1.83	5yr	1.24	1.65	2.12	2.66	3.31	4.13	4.62	5yr	3.65	4.45	5.09	6.02	6.71	5yr
10yr	0.49	0.77	0.97	1.32	1.72	2.20	10yr	1.48	1.95	2.56	3.21	3.99	4.94	5.58	10yr	4.37	5.36	6.13	7.21	7.95	10yr
25yr	0.58	0.93	1.18	1.64	2.18	2.82	25yr	1.88	2.45	3.29	4.12	5.11	6.27	7.14	25yr	5.55	6.87	7.85	9.15	9.94	25yr
50yr	0.67	1.08	1.39	1.95	2.62	3.41	50yr	2.26	2.90	3.98	4.98	6.15	7.52	8,62	50yr	6.66	8.29	9.46	10.97	11.78	50yr
100yr	0.78	1.26	1.63	2.30	3.14	4.11	100yr	2.71	3.45	4.81	6.02	7.42	9.03	1041	100yr	7.99	10.01	11.42	13.16	13.96	100yr
200yr	0.90	1.47	1.91	2.73	3.77	4.96	200yr	3.26	4.09	5.82	7.28	8.95 ^k	10.86	12 .59	200yr	9.61	12.10	13.79	15.78	16.56	200yr
500yr	1.11	1.82	2.37	3.44	4.82	6.37	500yr	4.16	5.13	7.48	9.36	11.47	13.87	16.18	500yr	12.28	15.55	17.69	20.09	20.75	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.24	0.37	0.45	0.61	0.75	0.90	1yr	0.65	0.88	1.04	1.40	1.85	2.37	2.65	1yr	2.09	2.55	2.95	3.51	4.02	1yr
2yr	0.34	0.53	0.65	0.89	1.09	1.29	2yr	0.94	1.26	1.48	1.96	2.53	3.15	3.47	2yr	2.79	3.34	3.80	4.54	5.16	2yr
5yr	0.39	0.60	0.75	1.02	1.30	1.55	5yr	1.12	1.52	1.76	2.31	2.95	3.77	4.19	5yr	3.34	4.03	4.55	5.67	6.07	5yr
10yr	0.43	0.67	0.83	1.16	1.50	1.77	10yr	1.29	1.73	2.00	2.61	3.31	4.29	4.86	10yr	3.79	4.67	5.20	6.16	6.86	10yr
25yr	0.50	0.76	0.95	1.35	1.78	2.09	25yr	1.54	2.05	2.38	3.08	3.85	5.10	5.92	25yr	4.52	5.69	6.20	7.36	8.06	25yr
50yr	0.55	0.84	1.05	1.51	2.03	2.38	50yr	1.75	2.32	2.70	3.48	4.33	5.89	6.89	50yr	5.21	6.63	7.10	8.43	9.11	50yr
100yr	0.62	0.93	1.16	1.68	2.31	2.70	100yr	1.99	2.64	3.07	3.94	4.87	6.79	8.05	100yr	6.01	7.74	8.14	9.68	10.27	100yr
200yr	0.68	1.02	1.29	1.87	2.61	3.08	200yr	2.26	3.01	3.49	4.47	5.47	7.87	9.43	200yr	6.97	9.07	9.30	11.13	11.61	200yr

precip.eas.cornell.edu/#/product/xprecip_results



NOAA Atlas 14, Volume 10, Version 3 Location name: Walpole, Massachusetts, USA* Latitude: 42.1474°, Longitude: -71.2538° Elevation: m/ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-k	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹													
Duration				Average	recurrence	interval (y	ears)							
Duration	1	2	5	10	25	50	100	200	500	1000				
5-min	0.319 (0.243-0.411)	0.391 (0.297-0.503)	0.508 (0.385-0.656)	0.605 (0.456-0.788)	0.739 (0.543-1.01)	0.838 (0.607-1.18)	0.945 (0.670-1.38)	1.07 (0.717-1.60)	1.27 (0.818-1.96)	1.43 (0.906-2.26)				
10-min	0.452 (0.344-0.582)	0.554 (0.421-0.713)	0.720 (0.546-0.931)	0.857 (0.646-1.11)	1.05 (0.770-1.43)	1.19 (0.859-1.67)	1.34 (0.949-1.96)	1.52 (1.01-2.26)	1.79 (1.16-2.77)	2.03 (1.28-3.20)				
15-min	0.532 (0.405-0.684)	0.651 (0.495-0.839)	0.846 (0.642-1.09)	1.01 (0.761-1.31)	1.23 (0.906-1.69)	1.40 (1.01-1.96)	1.57 (1.12-2.31)	1.79 (1.19-2.66)	2.11 (1.36-3.26)	2.39 (1.51-3.76)				
30-min	0.728 (0.554-0.936)	0.896 (0.681-1.15)	1.17 (0.887-1.51)	1.40 (1.05-1.82)	1.71 (1.26-2.34)	1.94 (1.41-2.73)	2.19 (1.55-3.21)	2.49 (1.67-3.71)	2.95 (1.90-4.55)	3.33 (2.11-5.25)				
60-min	0.924 (0.703-1.19)	1.14 (0.867-1.47)	1.49 (1.13-1.93)	1.79 (1.35-2.32)	2.19 (1.61-3.00)	2.49 (1.80-3.49)	2.81 (1.99-4.12)	3.20 (2.14-4.76)	3.78 (2.44-5.83)	4.28 (2.71-6.74)				
2-hr	1.17 (0.897-1.50)	1.47 (1.13-1.89)	1.97 (1.50-2.52)	2.38 (1.80-3.07)	2.94 (2.17-4.00)	3.36 (2.44-4.68)	3.81 (2.72-5.55)	4.36 (2.92-6.42)	5.20 (3.37-7.93)	5.91 (3.75-9.22)				
3-hr	1.36 (1.04-1.73)	1.71 (1.31-2.18)	2.29 (1.75-2.93)	2.77 (2.11-3.57)	3.43 (2.55-4.65)	3.92 (2.87-5.45)	4.45 (3.19-6.46)	5.10 (3.43-7.48)	6.09 (3.95-9.25)	6.94 (4.41-10.7)				
6-hr	1.77 (1.37-2.24)	2.21 (1.71-2.80)	2.93 (2.25-3.72)	3.52 (2.70-4.50)	4.34 (3.24-5.83)	4.95 (3.63-6.81)	5.60 (4.03-8.04)	6.40 (4.32-9.28)	7.60 (4.95-11.4)	8.63 (5.50-13.2)				
12-hr	2.31 (1.80-2.90) <mark>2</mark>	2.82 (2.19-3:55)	3.67 (2.84-4.62)	4.36 ~(3.36~5.54)~	5.32 (3.89-7.08)	6.04 (4.45-8.22)	6.81 (4.90-9.64)	7.72 (5.23-11.1)	9.09 (5.94-13.5)	10.2 (6.56-15.5)				
24-hr	2.83 (2.21-3.53)	3.46 (2.71-4.32)	4.49 (3.50-5.63)	5.35 (4.15-6.74)	6.53 (4.93-8.63)	7.41 5.49-10.0)	8.35 (6.05-11.8)	9.50 (6.46-13.5)	11.2 (7.37-16.5)	12.7 (8.17-19.1)				
2-day	3.25 (2.56-4.02)	4.05 (3.19-5.03)	5.37 (4.21-6.68)	6.46 (5.04-8.08)	7.96 (6.05-10.5)	9.07 (6.78-12.2)	10.3 (7.53-14.5)	11.8 (8.06-16.6)	14.2 (9.35-20.7)	16.3 (10.5-24.2)				
3-day	3.56 (2.81-4.39)	4.43 (3.50-5.47)	5.86 (4.61-7.26)	7.04 (5.51-8.77)	8.67 (6.61-11.4)	9.86 (7.40-13.2)	11.2 (8.22-15.7)	12.9 (8.79-18.0)	15.5 (10.2-22.4)	17.8 (11.5-26.2)				
4-day	3.85 (3.05-4.73)	4.75 (3.76-5.85)	6.22 (4.91-7.69)	7.44 (5.84-9.24)	9.13 (6.98-11.9)	10.4 (7.79-13.8)	11.7 (8.64-16.3)	13.5 (9.22-18.8)	16.2 (10.7-23.3)	18.6 (12.0-27.2)				
7-day	4.64 (3.69-5.67)	5.58 (4.43-6.83)	7.11 (5.64-8.74)	8.39 (6.61-10.4)	10.1 (7.78-13.1)	11.4 (8.62-15.1)	12.8 (9.47-17.7)	14.6 (10.1-20.2)	17.4 (11.5-24.8)	19.8 (12.9-28.8)				
10-day	5.37 (4.29-6.55)	6.34 (5.06-7.73)	7.91 (6.29-9.68)	9.22 (7.29-11.3)	11.0 (8.47-14.2)	12.3 (9.32-16.2)	13.8 (10.2-18.8)	15.6 (10.7-21.4)	18.3 (12.1-25.9)	20.7 (13.4-29.8)				
20-day	7.52 (6.05-9.10)	8.55 (6.87-10.4)	10.2 (8.20-12.4)	11.6 (9.26-14.2)	13.6 (10.5-17.2)	15.0 (11.3-19.4)	16.5 (12.1-22.0)	18.3 (12.7-24.8)	20.7 (13.8-29.0)	22.7 (14.8-32.4)				
30-day	9.28 (7.49-11.2)	10.4 (8.35-12.5)	12.1 (9.75-14.7)	13.6 (10.9-16.6)	15.6 (12.1-19.6)	17.2 (13.0-21.9)	18.8 (13.7-24.6)	20.4 (14.2-27.5)	22.6 (15.1-31.4)	24.3 (15.9-34.4)				
45-day	11.5 (9.28-13.8)	12.6 (10.2-15.1)	14.5 (11.7-17.4)	16.0 (12.8-19.4)	18.1 (14.0-22.6)	19.8 (14.9-25.0)	21.4 (15.6-27.7)	23.0 (16.1-30.7)	24.9 (16.7-34.3)	26.3 (17.2-37.0)				
60-day	13.3 (10.8-15.9)	14.5 (11.7-17.3)	16.4 (13.2-19.7)	18.0 (14.5-21.7)	20.2 (15.6-25.0)	21.9 (16.6-27.5)	23.6 (17.1-30.3)	25.1 (17.6-33.4)	26.8 (18.0-36.8)	28.0 (18.3-39.1)				

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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PF graphical



PDS-based depth-duration-frequency (DDF) curves





NOAA Atlas 14, Volume 10, Version 3

Created (GMT): Tue May 9 18:11:29 2023

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Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial



Back to Top

US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer



NOAA Atlas 14, Volume 10, Version 3 Location name: Walpole, Massachusetts, USA* Latitude: 42.1474°, Longitude: -71.2538° Elevation: 138 ft** * source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sandra Pavlovic, Michael St. Laurent, Carl Trypaluk, Dale Unruh, Orlan Wilhite

NOAA, National Weather Service, Silver Spring, Maryland

PF_tabular | PF_graphical | Maps_&_aerials

PF tabular

PDS-b	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹									
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	3.83 (2.92-4.93)	4.69 (3.56-6.04)	6.10 (4.62-7.87)	7.26 (5.47-9.46)	8.87 (6.52-12.1)	10.1 (7.28-14.1)	11.3 (8.04-16.6)	12.9 (8.60-19.2)	15.2 (9.82-23.5)	17.2 (10.9-27.1)
10-min	2.71 (2.06-3.49)	3.32 (2.53-4.28)	4.32 (3.28-5.59)	5.14 (3.88-6.68)	6.28 (4.62-8.60)	7.12 (5.15-9.99)	(5.69-11.8)	9.12 (6.09-13.6)	10.8 (6.95-16.6)	12.2 (7.70-19.2)
15-min	2.13	2.60	3.38	4.03	4.92	5.58	6.30	7.15	8.44	9.54
	(1.62-2.74)	(1.98-3.36)	(2.57-4.38)	(3.04-5.24)	(3.62-6.74)	(4.04-7.83)	(4.46-9.23)	(4.78-10.6)	(5.45-13.0)	(6.04-15.0)
30-min	1.46	1.79	2.34	2.79	3.42	3.88	4.38	4.98	5.89	6.66
	(1.11-1.87)	(1.36-2.31)	(1.77-3.02)	(2.11-3.63)	(2.52-4.68)	(2.81-5.45)	(3.11-6.43)	(3.33-7.42)	(3.80-9.09)	(4.22-10.5)
60-min	0.924	1.14	1.49	1.79	2.19	2.49	2.81	3.20	3.78	4.28
	(0.703-1.19)	(0.867-1.47)	(1.13-1.93)	(1.35-2.32)	(1.61-3.00)	(1.80-3.49)	(1.99-4.12)	(2.14-4.76)	(2.44-5.83)	(2.71-6.74)
2-hr	0.586	0.736	0.983	1.19	1.47	1.68	1.90	2.18	2.60	2.96
	(0.448-0.748)	(0.563-0.942)	(0.749-1.26)	(0.901-1.53)	(1.09-2.00)	(1.22-2.34)	(1.36-2.78)	(1.46-3.21)	(1.68-3.97)	(1.88-4.61)
3-hr	0.451	0.569	0.762	0.923	1.14	1.31	1.48	1.70	2.03	2.31
	(0.347-0.575)	(0.437-0.726)	(0.583-0.975)	(0.702-1.19)	(0.849-1.55)	(0.954-1.81)	(1.06-2.15)	(1.14-2.49)	(1.32-3.08)	(1.47-3.58)
6-hr	0.295	0.368	0.488	0.588	0.724	0.826	0.935	1.07	1.27	1.44
	(0.228-0.373)	(0.284-0.467)	(0.376-0.620)	(0.450-0.751)	(0.540-0.973)	(0.606-1.14)	(0.672-1.34)	(0.720-1.55)	(0.826-1.91)	(0.919-2.21)
12-hr	0.191	0.234	0.304	0.362	0.441	0.501	0.564	0.640	0.754	0.850
	(0.149-0.240)	(0.182-0.294)	(0.235-0.383)	(0.278-0.459)	(0.331-0.587)	(0.369-0.682)	(0.406-0.800)	(0.434-0.919)	(0.493-1.12)	(0.544-1.29)
24-hr	0.117	0.144	0.187	0.223	0.272	0.308	0.348	0.395	0.468	0.530
	(0.092-0.146)	(0.112-0.180)	(0.145-0.234)	(0.172-0.280)	(0.205-0.359)	(0.228-0.417)	(0.252-0.489)	(0.269-0.562)	(0.307-0.688)	(0.340-0.794)
2-day	0.067	0.084	0.111	0.134	0.165	0.188	0.214	0.246	0.296	0.339
	(0.053-0.083)	(0.066-0.104)	(0.087-0.139)	(0.104-0.168)	(0.126-0.218)	(0.141-0.254)	(0.156-0.301)	(0.167-0.346)	(0.194-0.430)	(0.218-0.503)
3-day	0.049	0.061	0.081	0.097	0.120	0.136	0.155	0.178	0.215	0.247
	(0.039-0.060)	(0.048-0.076)	(0.063-0.100)	(0.076-0.121)	(0.091-0.157)	(0.102-0.183)	(0.114-0.217)	(0.122-0.249)	(0.141-0.311)	(0.159-0.364)
4-day	0.040	0.049	0.064	0.077	0.095	0.107	0.122	0.140	0.168	0.193
	(0.031-0.049)	(0.039-0.060)	(0.051-0.080)	(0.060-0.096)	(0.072-0.124)	(0.081-0.144)	(0.089-0.170)	(0.096-0.195)	(0.111-0.242)	(0.125-0.283)
7-day	0.027	0.033	0.042	0.049	0.060	0.068	0.076	0.087	0.103	0.118
	(0.021-0.033)	(0.026-0.040)	(0.033-0.051)	(0.039-0.061)	(0.046-0.078)	(0.051-0.089)	(0.056-0.105)	(0.059-0.120)	(0.068-0.147)	(0.076-0.171)
10-day	0.022	0.026	0.032	0.038	0.045	0.051	0.057	0.064	0.076	0.086
	(0.017-0.027)	(0.021-0.032)	(0.026-0.040)	(0.030-0.047)	(0.035-0.058)	(0.038-0.067)	(0.042-0.078)	(0.044-0.089)	(0.050-0.107)	(0.055-0.124)
20-day	0.015	0.017	0.021	0.024	0.028	0.031	0.034	0.038	0.043	0.047
	(0.012-0.018)	(0.014-0.021)	(0.017-0.025)	(0.019-0.029)	(0.021-0.035)	(0.023-0.040)	(0.025-0.045)	(0.026-0.051)	(0.028-0.060)	(0.030-0.067)
30-day	0.012	0.014	0.016	0.018	0.021	0.023	0.026	0.028	0.031	0.033
	(0.010-0.015)	(0.011-0.017)	(0.013-0.020)	(0.015-0.022)	(0.016-0.027)	(0.017-0.030)	(0.018-0.034)	(0.019-0.038)	(0.021-0.043)	(0.022-0.047)
45-day	0.010	0.011	0.013	0.014	0.016	0.018	0.019	0.021	0.023	0.024
	(0.008-0.012)	(0.009-0.014)	(0.010-0.016)	(0.011-0.017)	(0.012-0.020)	(0.013-0.023)	(0.014-0.025)	(0.014-0.028)	(0.015-0.031)	(0.015-0.034)
60-day	0.009	0.010	0.011	0.012	0.014	0.015	0.016	0.017	0.018	0.019
	(0.007-0.011)	(0.008-0.012)	(0.009-0.013)	(0.010-0.015)	(0.010-0.017)	(0.011-0.019)	(0.011-0.021)	(0.012-0.023)	(0.012-0.025)	(0.012-0.027)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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PF graphical







Duration					
5-min	2-day				
10-min	— 3-day				
15-min	— 4-day				
30-min	— 7-day				
60-min	— 10-day				
— 2-hr	— 20-day				
— 3-hr	— 30-day				
— 6-hr	— 45-day				
- 12-hr	— 60-day				
- 24-hr					

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Maps & aerials

Small scale terrain



Large scale terrain





Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

Disclaimer

APPENDIX G: OPERATION AND MAINTENANCE

- > STORMWATER OPERATION AND MAINTENANCE PLAN
- > <u>INSPECTION REPORT</u>
- > INSPECTION AND MAINTENANCE LOG FORM
- > LONG-TERM POLLUTION PREVENTION PLAN
- ILLICIT DISCHARGE STATEMENT
- > <u>SPILL PREVENTION</u>
- > MANUFACTURER'S INSPECTION AND MAINTENANCE MANUALS

STORMWATER OPERATION AND MAINTENANCE PLAN

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA

RESPONSIBLE PARTY DURING CONSTRUCTION:

KIG/Silverstrand Walpole, LLC Attn: Sean Henry 257 Hillside Avenue Needham, MA 02492 Phone: 781-957-6102

RESPONSIBLE PARTY POST CONSTRUCTION:

KIG/Silverstrand Walpole, LLC Attn: Sean Henry 257 Hillside Avenue Needham, MA 02492 Phone: 781-957-6102

Construction Phase

During the construction phase, all erosion control devices and measures shall be maintained in accordance with the final record plans, local/state approvals and conditions, the EPA Construction General Permit and the Stormwater Pollution Prevention Plan (SWPPP) if applicable. Additionally, the maintenance of all erosion / siltation control measures during construction shall be the responsibility of the general contractor. Contact information of the OWNER and CONTRACTOR shall be listed in the SWPPP for this site. The SWPPP also includes information regarding construction period allowable and illicit discharges, housekeeping and emergency response procedures. Upon proper notice to the property owner, the Town or its authorized designee shall be allowed to enter the property at a reasonable time and in a reasonable manner for the purposes of inspection.

Post Development Controls

Once construction is completed, the post development stormwater controls are to be operated and maintained in compliance with the following permanent procedures (note that the continued implementation of these procedures shall be the responsibility of the Owner or its assignee):

- 1. Parking lots and on-site driveways: Sweep at least two (2) times per year and on a more frequent basis depending on sanding operations. All resulting sweepings shall be collected and properly disposed of off site in accordance with MADEP and other applicable requirements.
- 2. Catch basins, yard drains, trench drains, manholes and piping: Inspect two (2) times per year and at the end of foliage and snow-removal seasons. These features shall be cleaned two (2) times per year or whenever the depth of deposits is greater than or equal to one

half the depth from the bottom of the invert of the lowest pipe in the catch basin or underground system. Accumulated sediment and hydrocarbons present must be removed and properly disposed of off site in accordance with MADEP and other applicable requirements.

- 3. Water Quality Unit (Proprietary Separator): Follow manufacturer's recommendations (attached).
- 4. Underground Infiltration Basins: Preventative maintenance after every major storm event during the first three (3) months of operation and at least twice per year thereafter. Inspect structure and pretreatment BMP to ensure proper operation after every major storm event (generally equal or greater to 3.0 inches in 24 hours) for the first three months. The outlet of the basin, if any, shall be inspected for erosion and sedimentation, and rip-rap shall be promptly repaired in the case of erosion. Sediment collecting in the bottom of the basin shall be inspected twice annually, and removal shall commence any time the sediment reaches a depth of six inches anywhere in the basin. Any sediment removed shall be disposed of in accordance with MADEP and other applicable requirements.

All components of the stormwater system will be accessible by the owner or their assignee.

STORMWATER MANAGEMENT SYSTEM

POST-CONSTRUCTION INSPECTION REPORT

LOCATION:

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA

RESPONSIBLE PARTY:

KIG/Silverstrand Walpole, LLC Attn: Sean Henry 257 Hillside Avenue Needham, MA 02492 Phone: 781-957-6102

NAME OF INSPECTOR:	INSPECTION DATE:
Note Condition of the Following (sedimer	nt depth, debris, standing water, damage, etc.):
Catch Basins:	
Discharge Points/ Flared End Sections /	/ Rip Rap:
Infiltration Basin:	
water Quality Units:	
Other:	
other.	

Note Recommended Actions to be taken on the Following (sediment and/or debris removal, repairs, etc.):
Catch Basins:
Discharge Points / Flared End Sections / Rin Ran
Discharge Fonite / Flared Dia Sections / Rep Rap.
Infiltration Resin:
water Quality Units:
Other:
Other:
2
Comments:

STORMWATER INSPECTI	ON AND MAINTENA	NCE LOC	G FORM		
Proposed Multi-Family Development					
981, 989 & 1015 East Street – Walpole, MA					
Stormwater Management	Responsible Party	Date	Naintenance Activity		
Practice			Performed		

LONG-TERM POLLUTION PREVENTION PLAN

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA

RESPONSIBLE PARTY DURING CONSTRUCTION:

KIG/Silverstrand Walpole, LLC Attn: Sean Henry 257 Hillside Avenue Needham, MA 02492 Phone: 781-957-6102

RESPONSIBLE PARTY POST CONSTRUCTION:

KIG/Silverstrand Walpole, LLC Attn: Sean Henry 257 Hillside Avenue Needham, MA 02492 Phone: 781-957-6102

For this site, the Long-Term Pollution Prevention Plan will consist of the following:

- The property owner shall be responsible for "good housekeeping" including proper periodic maintenance of building and pavement areas, curbing, landscaping, etc.
- Proper storage and removal of solid waste (dumpsters).
- Sweeping of driveways a minimum of twice per year with a commercial cleaning unit. Any sediment removed shall be disposed of in accordance with applicable local and state requirements.
- Regular inspections and maintenance of Stormwater Management System as noted in the "O&M Plan".
- Snow removal shall be the responsibility of the property owner. Snow shall not be plowed, dumped and/or placed in forebays, infiltration basins or similar stormwater controls. Salting and/or sanding of pavement / walkway areas during winter conditions shall only be done in accordance with all state/local requirements and approvals.
- In no case shall snow be disposed of or stored in resource areas (wetlands, floodplain, streams or other water bodies).
- If necessary, stockpiled snow will be removed from the Site and disposed of at an off-site location in accordance with all local, state and federal regulations.

• The amount of sand and deicing chemicals shall be kept at the minimum amount required to provide safe pedestrian and vehicle travel.

OPERATON AND MAINTENANCE TRAINING PROGRAM

The Owner will coordinate an annual in-house training session to discuss the Operations and Maintenance Plan, the Long-Term Pollution Prevention Plan, and the Spill Prevention Plan and response procedures. Annual training will include the following:

Discuss the Operations and Maintenance Plan

- Explain the general operations of the stormwater management system and its BMPs
- Identify potential sources of stormwater pollution and measures / methods of reducing or eliminating that pollution
- Emphasize good housekeeping measures

Discuss the Spill Prevention and Response Procedures

- Explain the process in the event of a spill
- Identify potential sources of spills and procedures for cleanup and /or reporting and notification
- Complete a yearly inventory or Materials Safety Data sheets of all tenants and confirm that no potentially harmful chemicals are in use.

ILLICIT DISCHARGE STATEMENT

Certain types of non-stormwater discharges are allowed under the U.S. Environmental Protection Agency Construction General Permit. These types of discharges will be allowed under the conditions that no pollutants will be allowed to come in contact with the water prior to or after its discharge. The control measures which have been outlined previously in this LTPPP will be strictly followed to ensure that no contamination of these non-storm water discharges takes place. Any existing illicit discharges, if discovered during the course of the work, will be reported to MassDEP and the local DPW, as applicable, to be addressed in accordance with their respective policies. No illicit discharges will be allowed in conjunction with the proposed improvements.

SPILL PREVENTION AND RESPONSE PROCEDURES (POST CONSTRUCTION)

In order to prevent or minimize the potential for a spill of Hazardous Substances or Oil or come into contact with stormwater, the following steps will be implemented:

- 1. All Hazardous Substances or Oil (such as pesticides, petroleum products, fertilizers, detergents, acids, paints, paint solvents, cleaning solvents, etc.) will be stored in a secure location, with their lids on, preferably under cover, when not in use.
- 2. The minimum practical quantity of all such materials will be kept on site.
- 3. A spill control and containment kit (containing, for example, absorbent materials, acid neutralizing powder, brooms, dust pans, mops, rags, gloves, goggles, plastic and metal trash containers, etc.) will be provided on site.
- 4. Manufacturer's recommended methods for spill cleanup will be clearly posted and site personnel will be trained regarding these procedures and the location of the information and cleanup supplies.
- 5. It is the OWNER's responsibility to ensure that all Hazardous Waste on site is disposed of properly by a licensed hazardous material disposal company. The OWNER is responsible for not exceeding Hazardous Waste storage requirements mandated by the EPA or state and local authorities.

In the event of a spill of Hazardous Substances or Oil, the following procedures should be followed:

- 1. All measures should be taken to contain and abate the spill and to prevent the discharge of the Hazardous Substance or Oil to stormwater or off-site. (The spill area should be kept well ventilated and personnel should wear appropriate protective clothing to prevent injury from contact with the Hazardous Substances.)
- 2. For spills of less than five (5) gallons of material, proceed with source control and containment, clean-up with absorbent materials or other applicable means unless an imminent hazard or other circumstances dictate that the spill should be treated by a professional emergency response contractor.
- For spills greater than five (5) gallons of material immediately contact the MADEP at the toll-free 24-hour statewide emergency number: 1-888-304-1133, the local fire department (9-1-1) and an approved emergency response contractor. Provide information on the type of material spilled, the location of the spill, the quantity spilled, and the time of the spill to the emergency response contractor or coordinator, and proceed with prevention, containment and/or clean-up if so desired. (Use the form provided, or similar).
- 4. If there is a Reportable Quantity (RQ) release, then the National Response Center should be notified immediately at (800) 424-8802; within 14 days a report should be submitted to the EPA regional office describing the release, the date and circumstances of the release and the steps taken to prevent another release. This Pollution Prevention Plan should be updated to reflect any such steps or actions taken and measures to prevent the same from reoccurring.

SPILL PREVENTION CONTROL AND COUNTERMEASURE FORM

Proposed Multi-Family Development 981, 989 & 1015 East Street Walpole, MA

Where a release containing a hazardous substance occurs, the following steps shall be taken by the facility manager and/or supervisor:

- 1. Immediately notify the Walpole Fire Department (at 9-1-1)
- 2. All measures must be taken to contain and abate the spill and to prevent the discharge of the pollutant(s) to off-site locations, receiving waters, wetlands and/or resource areas.
- 3. Notify the Walpole Board of Health at (508) 660-7321 and the Walpole Conservation Commission at (508) 660-7268.
- 4. Provide documentation from licensed contractor showing disposal and cleanup procedures were completed as well as details on chemicals that were spilled to the Town of Walpole Board of Health and Conservation Commission.

Date of spill:_____ Time:____

Reported By:_____

Weather Conditions:

Material Spilled	Location of Spill	Approximate Quantity of Spill (in gallons)	Agency(s) Notified	Date of Notification

Cause of Spill.		
Aeasures Taken to Clean up Spill:		
Sype of equipment:	Make:	Size:
icense or S/N:	_	
Location and Method of Disposal	instituted to prevent a simila	ar occurrence from recurring:
Additional Contact Numbers:		
DEPARTME PHONE: 1-88	NT OF ENVIRONMENT 88-304-1133	TAL PROTECTION (DEP) EMERGENCY
NATIONAL	RESPONSE CENTER PH	HONE: (800) 424-8802
• U.S. ENVIRO	ONMENTAL PROTECTI	ON AGENCYPHONE: (888) 372-7341


Save Valuable Land and Protect Water Resources

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Isolator[®] Row O&M Manual

 $\mathsf{StormTech}^{\scriptscriptstyle \otimes}$ Chamber System for Stormwater Management

1.0 The Isolator® Row

1.1 INTRODUCTION

An important component of any Stormwater Pollution Prevention Plan is inspection and maintenance. The StormTech Isolator Row is a patented technique to inexpensively enhance Total Suspended Solids (TSS) removal and provide easy access for inspection and maintenance.



Looking down the Isolator Row from the manhole opening, woven geotextile is shown between the chamber and stone base.

1.2 THE ISOLATOR ROW

The Isolator Row is a row of StormTech chambers, either SC-310, SC-310-3, SC-740, DC-780, MC-3500 or MC-4500 models, that is surrounded with filter fabric and connected to a closely located manhole for easy access. The fabric-wrapped chambers provide for settling and filtration of sediment as storm water rises in the Isolator Row and ultimately passes through the filter fabric. The open bottom chambers and perforated sidewalls (SC-310, SC-310-3 and SC-740 models) allow storm water to flow both vertically and horizontally out of the chambers. Sediments are captured in the Isolator Row protecting the storage areas of the adjacent stone and chambers from sediment accumulation.

Two different fabrics are used for the Isolator Row. A woven geotextile fabric is placed between the stone and the Isolator Row chambers. The tough geotextile provides a media for storm water filtration and provides a durable surface for maintenance operations. It is also designed to prevent scour of the underlying stone and remain intact during high pressure jetting. A non-woven fabric is placed over the chambers to provide a filter media for flows passing through the perforations in the sidewall of the chamber. The non-woven fabric is not required over the DC-780, MC-3500 or MC-4500 models as these chambers do not have perforated side walls.

The Isolator Row is typically designed to capture the "first flush" and offers the versatility to be sized on a volume basis or flow rate basis. An upstream manhole not only provides access to the Isolator Row but typically includes a high flow weir such that storm water flowrates or volumes that exceed the capacity of the Isolator Row overtop the over flow weir and discharge through a manifold to the other chambers.

The Isolator Row may also be part of a treatment train. By treating storm water prior to entry into the chamber system, the service life can be extended and pollutants such as hydrocarbons can be captured. Pre-treatment best management practices can be as simple as deep sump catch basins, oil-water separators or can be innovative storm water treatment devices. The design of the treatment train and selection of pretreatment devices by the design engineer is often driven by regulatory requirements. Whether pretreatment is used or not, the Isolator Row is recommended by StormTech as an effective means to minimize maintenance requirements and maintenance costs.

Note: See the StormTech Design Manual for detailed information on designing inlets for a StormTech system, including the Isolator Row.

StormTech Isolator Row with Overflow Spillway (not to scale)



2.0 Isolator Row Inspection/Maintenance



2.1 INSPECTION

The frequency of Inspection and Maintenance varies by location. A routine inspection schedule needs to be established for each individual location based upon site specific variables. The type of land use (i.e. industrial, commercial, residential), anticipated pollutant load, percent imperviousness, climate, etc. all play a critical role in determining the actual frequency of inspection and maintenance practices.

At a minimum, StormTech recommends annual inspections. Initially, the Isolator Row should be inspected every 6 months for the first year of operation. For subsequent years, the inspection should be adjusted based upon previous observation of sediment deposition.

The Isolator Row incorporates a combination of standard manhole(s) and strategically located inspection ports (as needed). The inspection ports allow for easy access to the system from the surface, eliminating the need to perform a confined space entry for inspection purposes.

If upon visual inspection it is found that sediment has accumulated, a stadia rod should be inserted to determine the depth of sediment. When the average depth of sediment exceeds 3 inches throughout the length of the Isolator Row, clean-out should be performed.

2.2 MAINTENANCE

The Isolator Row was designed to reduce the cost of periodic maintenance. By "isolating" sediments to just one row, costs are dramatically reduced by eliminating the need to clean out each row of the entire storage bed. If inspection indicates the potential need for maintenance, access is provided via a manhole(s) located on the end(s) of the row for cleanout. If entry into the manhole is required, please follow local and OSHA rules for a confined space entries.



Examples of culvert cleaning nozzles appropriate for Isolator Row maintenance. (These are not StormTech products.)

Maintenance is accomplished with the JetVac process. The JetVac process utilizes a high pressure water nozzle to propel itself down the Isolator Row while scouring and suspending sediments. As the nozzle is retrieved, the captured pollutants are flushed back into the manhole for vacuuming. Most sewer and pipe maintenance companies have vacuum/JetVac combination vehicles. Selection of an appropriate JetVac nozzle will improve maintenance efficiency. Fixed nozzles designed for culverts or large diameter pipe cleaning are preferable. Rear facing jets with an effective spread of at least 45" are best. Most JetVac reels have 400 feet of hose allowing maintenance of an Isolator Row up to 50 chambers long. The JetVac process shall only be performed on StormTech Isolator Rows that have AASHTO class 1 woven geotextile (as specified by StormTech) over their angular base stone.



NOTE: NON-WOVEN FABRIC IS ONLY REQUIRED OVER THE INLET PIPE CONNECTION INTO THE END CAP FOR DC-780, MC-3500 AND MC-4500 CHAMBER MODELS AND IS NOT REQUIRED OVER THE ENTIRE ISOLATOR ROW.

StormTech Isolator Row (not to scale)

3.0 Isolator Row Step By Step Maintenance Procedures

Step 1) Inspect Isolator Row for sediment

- A) Inspection ports (if present)
 - i. Remove lid from floor box frame
 - ii. Remove cap from inspection riser
 - Using a flashlight and stadia rod, measure depth of sediment and record results on maintenance log.
 - iv. If sediment is at, or above, 3 inch depth proceed to Step 2. If not proceed to step 3.
- B) All Isolator Rows
 - i. Remove cover from manhole at upstream end of Isolator Row

StormTech Isolator Row (not to scale)



- ii. Using a flashlight, inspect down Isolator Row through outlet pipe1. Mirrors on poles or cameras may be used to avoid a confined space entry2. Follow OSHA regulations for confined space entry if entering manhole
- iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches) proceed to Step 2. If not proceed to Step 3.
- Step 2) Clean out Isolator Row using the JetVac process
 - A) A fixed culvert cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
 - B) Apply multiple passes of JetVac until backflush water is clean
 - C) Vacuum manhole sump as required
- Step 3) Replace all caps, lids and covers, record observations and actions
- Step 4) Inspect & clean catch basins and manholes upstream of the StormTech system

Sample Maintenance Log

	Stadia Rod Readings		Oculiances		
Date	Fixed point to chamber bottom (1)	Fixed point to top of sediment (2)	Depth (1) - (2)	Observations/Actions	Inspector
3/15/01	6.3 ft.	none		New installation. Fixed point is Cl frame at grade	djm
9/24/01		6.2	0.1 ft.	Some grit felt	sm
6/20/03		5.8	0.5 ft.	Mucky feel, debris visible in manhole and in Isolator row, maintenance due	rv
7/7/03	6.3 ft.		0	System jetted and vacuumed	djm





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CDS® Inspection and Maintenance Guide





Maintenance

The CDS system should be inspected at regular intervals and maintained when necessary to ensure optimum performance. The rate at which the system collects pollutants will depend more heavily on site activities than the size of the unit. For example, unstable soils or heavy winter sanding will cause the grit chamber to fill more quickly but regular sweeping of paved surfaces will slow accumulation.

Inspection

Inspection is the key to effective maintenance and is easily performed. Pollutant transport and deposition may vary from year to year and regular inspections will help ensure that the system is cleaned out at the appropriate time. At a minimum, inspections should be performed twice per year (e.g. spring and fall) however more frequent inspections may be necessary in climates where winter sanding operations may lead to rapid accumulations, or in equipment washdown areas. Installations should also be inspected more frequently where excessive amounts of trash are expected.

The visual inspection should ascertain that the system components are in working order and that there are no blockages or obstructions in the inlet and separation screen. The inspection should also quantify the accumulation of hydrocarbons, trash, and sediment in the system. Measuring pollutant accumulation can be done with a calibrated dipstick, tape measure or other measuring instrument. If absorbent material is used for enhanced removal of hydrocarbons, the level of discoloration of the sorbent material should also be identified during inspection. It is useful and often required as part of an operating permit to keep a record of each inspection. A simple form for doing so is provided.

Access to the CDS unit is typically achieved through two manhole access covers. One opening allows for inspection and cleanout of the separation chamber (cylinder and screen) and isolated sump. The other allows for inspection and cleanout of sediment captured and retained outside the screen. For deep units, a single manhole access point would allows both sump cleanout and access outside the screen.

The CDS system should be cleaned when the level of sediment has reached 75% of capacity in the isolated sump or when an appreciable level of hydrocarbons and trash has accumulated. If absorbent material is used, it should be replaced when significant discoloration has occurred. Performance will not be impacted until 100% of the sump capacity is exceeded however it is recommended that the system be cleaned prior to that for easier removal of sediment. The level of sediment is easily determined by measuring from finished grade down to the top of the sediment pile. To avoid underestimating the level of sediment in the chamber, the measuring device must be lowered to the top of the sediment pile carefully. Particles at the top of the pile typically offer less resistance to the end of the rod than consolidated particles toward the bottom of the pile. Once this measurement is recorded, it should be compared to the as-built drawing for the unit to determine weather the height of the sediment pile off the bottom of the sump floor exceeds 75% of the total height of isolated sump.

Cleaning

Cleaning of a CDS systems should be done during dry weather conditions when no flow is entering the system. The use of a vacuum truck is generally the most effective and convenient method of removing pollutants from the system. Simply remove the manhole covers and insert the vacuum hose into the sump. The system should be completely drained down and the sump fully evacuated of sediment. The area outside the screen should also be cleaned out if pollutant build-up exists in this area.

In installations where the risk of petroleum spills is small, liquid contaminants may not accumulate as quickly as sediment. However, the system should be cleaned out immediately in the event of an oil or gasoline spill should be cleaned out immediately. Motor oil and other hydrocarbons that accumulate on a more routine basis should be removed when an appreciable layer has been captured. To remove these pollutants, it may be preferable to use absorbent pads since they are usually less expensive to dispose than the oil/water emulsion that may be created by vacuuming the oily layer. Trash and debris can be netted out to separate it from the other pollutants. The screen should be power washed to ensure it is free of trash and debris.

Manhole covers should be securely seated following cleaning activities to prevent leakage of runoff into the system from above and also to ensure that proper safety precautions have been followed. Confined space entry procedures need to be followed if physical access is required. Disposal of all material removed from the CDS system should be done in accordance with local regulations. In many jurisdictions, disposal of the sediments may be handled in the same manner as the disposal of sediments removed from catch basins or deep sump manholes.



CDS Model	Diameter		Distance from Water Surface to Top of Sediment Pile		Sediment Storage Capacity	
	ft	m	ft	m	У³	m³
CDS1515	3	0.9	3.0	0.9	0.5	0.4
CDS2015	4	1.2	3.0	0.9	0.9	0.7
CDS2015	5	1.3	3.0	0.9	1.3	1.0
CDS2020	5	1.3	3.5	1.1	1.3	1.0
CDS2025	5	1.3	4.0	1.2	1.3	1.0
CDS3020	6	1.8	4.0	1.2	2.1	1.6
CDS3025	6	1.8	4.0	1.2	2.1	1.6
CDS3030	6	1.8	4.6	1.4	2.1	1.6
CDS3035	6	1.8	5.0	1.5	2.1	1.6
CDS4030	8	2.4	4.6	1.4	5.6	4.3
CDS4040	8	2.4	5.7	1.7	5.6	4.3
CDS4045	8	2.4	6.2	1.9	5.6	4.3
CDS5640	10	3.0	6.3	1.9	8.7	6.7
CDS5653	10	3.0	7.7	2.3	8.7	6.7
CDS5668	10	3.0	9.3	2.8	8.7	6.7
CDS5678	10	3.0	10.3	3.1	8.7	6.7

Table 1: CDS Maintenance Indicators and Sediment Storage Capacities



Support

- Drawings and specifications are available at www.contechstormwater.com.
- Site-specific design support is available from our engineers.
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CDS Inspection & Maintenance Log

CDS Mode	l:		Lo	ocation:	
Date	Water depth to sediment ¹	Floatable Layer Thickness ²	Describe Maintenance Performed	Maintenance Personnel	Comments

1. The water depth to sediment is determined by taking two measurements with a stadia rod: one measurement from the manhole opening to the top of the sediment pile and the other from the manhole opening to the water surface. If the difference between these measurements is less than the values listed in table 1 the system should be cleaned out. Note: to avoid underestimating the volume of sediment in the chamber, the measuring device must be carefully lowered to the top of the sediment pile.

2. For optimum performance, the system should be cleaned out when the floating hydrocarbon layer accumulates to an appreciable thickness. In the event of an oil spill, the system should be cleaned immediately.