Memo

To:	Bernie Marshall, Superintendent
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From: Raymond Willis, P.E.

CC: David Hale, Omni Properties, LLC

Date: December 17, 2020

Re: Summer Street Development, Walpole, MA

As requested, Onsite Engineering has prepared this memorandum to detail the preliminary design of the sewage collection system servicing the proposed Summer Street development located in Walpole, Massachusetts. The collection system, as currently proposed, utilizes a combination of gravity collection sewer and three (3) sewage pump stations, which are connected to a common force main system. The common force main from the pump stations would connect to a segment of gravity sewer located at the entrance to the site, which would then flow by gravity to the Town's sewage collection system within Summer Street.

The gravity collection system within the site consists of four (4) sewer service areas. For each service area, we inventoried the number of connected uses to determine the anticipated average day sewage generation, the maximum day sewage generation, and the peak hour flow rate. The average and maximum day sewage generation are based on design flow criteria established in 310 CMR 15.000, Title 5, which uses a 2 to 1 relationship between the maximum day and average day sewage generation. For this project, in order to calculate the peak hour flow rate, we utilized Title 5 design flow criteria to determine the maximum day sewage generation and then used that information in conjunction with the "Relation of Extreme Discharges on Maximum and Minimum Days to the Average Daily Discharge of Domestic Sewage" graph from Technical Release 16 (TR-16) prepared by the New England Interstate Water Pollution Control Commission (NEIWPPC), which is the industry standard protocol to complete exercises such as this to determine the remaining flow criteria for the sewer system.

Using the aforementioned graph, we first determined the ratios between peak hour, maximum day and average day flows for a system of this size. From the graph, those ratios are 5.6 to 3 to 1 respectively. It is important to note that in TR-16, at flows less than 100,000 gallons per day, the peak day to average day flow ratio is 3 to 1, which is not as conservative as the required Title 5 ratio noted above. Therefore, since Title 5 maximum day flow is a more conservative approach than that of the TR-16 method, we had to adjust the peak hour to average day ratio in order keep the maximum day to average day ratio at no more than 2



to 1. Therefore, the Title 5 adjusted peak hour to average day flow ratio was calculated to be 3.7 to 1 rather than 5.6 to 1.

Using the Proposed Subdivision/Overall Plan as a basemap (PDF attached), we have annotated the drawings accordingly to designate the four service areas described herein. A summary of these service areas are as follows:

Service Area #1

Calculated Title 5 Design Flow: 49,940 gallons Maximum Day Flow: 49,940 gallons Average Day Flow: 24,970 gallons per day Peak Hour Flow Rate: 64.2 gallons per minute

Pump Station Criteria

- 8 foot inside diameter wet well
- Triplex submersible pump system
- 126 gpm target pumping rate

Service Area #2

Calculated Title 5 Design Flow: 5,720 gallons Maximum Day Flow: 5,720 gallons Average Day Flow: 2,860 gallons per day Peak Hour Flow Rate: 7.3 gallons per minute

Pump Station Criteria

- 5 foot inside diameter wet well
- Duplex submersible pump system
- 90 gpm target pumping rate

Service Area #3

Calculated Title 5 Design Flow: 3,300 gallons Maximum Day Flow: 3,300 gallons Average Day Flow: 1,650 gallons per day Peak Hour Flow Rate: 4.2 gallons per minute

Pump Station Criteria

- 5 foot inside diameter wet well
- Duplex submersible pump system
- 115 gpm target pumping rate



Service Area #4

Calculated Title 5 Design Flow: 1,430 gallons Maximum Day Flow: 1,430 gallons Average Day Flow: 715 gallons per day Peak Hour Flow: 1.8 gallons per minute

Overall Site

Calculated Title 5 Design Flow: 60,390 gallons Maximum Day Flow: 60,390 gallons Average Day Flow: 30,195 gallons per day Peak Hour Flow Rate: 77.6 gallons per minute

Based on existing site topography, proposed site grading, and the location of the municipal sewer connection, the as proposed configuration of the sewage pump stations' force main piping is consistent with design strategies used for low pressure sewage collection systems, which are widely used throughout New England and the United States. A distinct advantage to configuring the force mains in this manner is that it reduces the overall length of force main required, therefore, reducing the sewage's detention time in the force main system.

Given this design strategy, we requested that the pump system manufacturer prepare a model of the sewage pump station operations. As summarized in modeling reports prepared by Pentair, based on Pentair's experience under normal operating conditions, it is anticipated that two of the three pump stations would be in operation at a given time. Under this operation scenario, Pentair modeled (reports attached) the largest pump station (Pump Station #1) running with each smaller pump station (Pump Station #2 and Pump Station #3) running as well. In addition, Pentair modeled the anticipated flow rates from the possible scenario of all three stations in simultaneous operation, if such an event would occur. The results of these analyses are as follows:

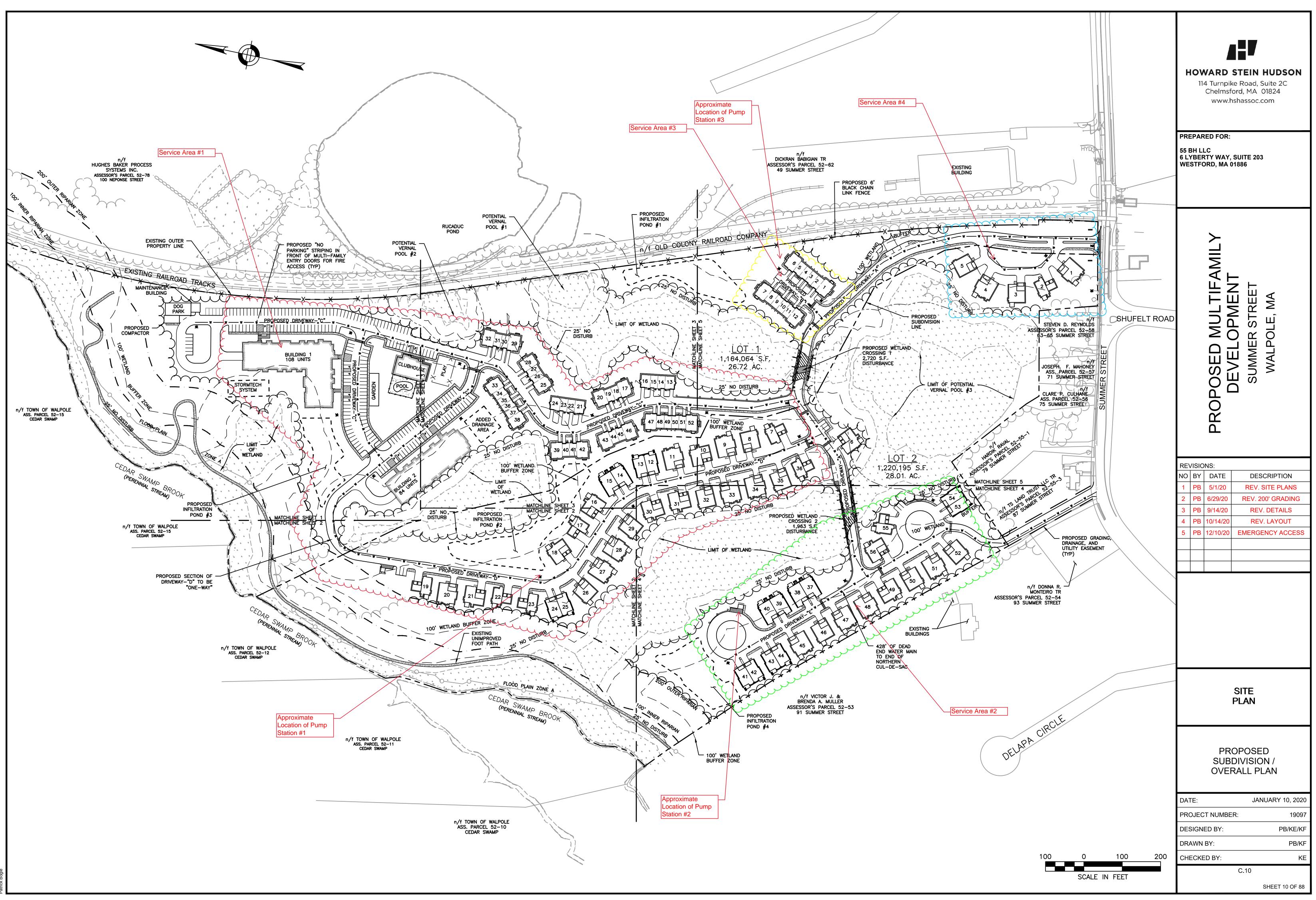
Pump Station #1 and Pump Station #2 simultaneous operation: 224 gpm Pump Station #1 and Pump Station #3 simultaneous operation: 181 gpm Pump Station #1, Pump Station #2, and Pump Station #3 simultaneous operation: 252 gpm

In summary, based on the preliminary design information we have at this time, the volume of sewage generated by the site is anticipated to be 30,195 gallons per day on average, with a maximum day sewage generation of 60,390 gallons. The corresponding peak hour flow rate associated with the entire site is calculated to be approximately 77.6 gpm. The flow rates into the municipal sewer system associated with the operation of the pump stations are anticipated to range from 90 gpm (if the service area 2 station were running alone) up to 224 gpm under the simultaneous operation of the two larger pump stations from service areas 1 and 2. Under the limited occurrence scenario of all three pump stations operating simultaneously, the estimated flow rate from the site would be approximately 252 gpm.



Upon your review of this preliminary design memorandum, if you have any questions or require any additional information, please feel free to contact me at <u>rwillis@onsite-eng.com</u> or at (508) 553-0616, ext 701.



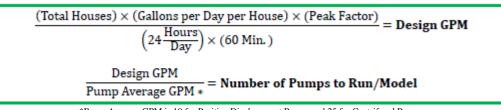


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LPS Design Report Guide

Determining Number of Pumps to Run/Model on LPS Layout:

The numbers of pumps to run/model on the LPS layout are determined from the following equation:



*Pump Average GPM is 10 for Positive Displacement Pumps and 25 for Centrifugal Pumps

Definition of Terms:

<u>Node Name</u> :	Software utilizes "nodes" to signify various types of items within the system. Nodes are referenced on supplied map entitled "Node Names." The following designations are used								
		for different kinds of nodes.							
	J= Junction Node O= Pump R= Reservoir, Lift Station, Treatment Plant								
<u>Pipe Name</u> :	Identify pipe see	ction connecting two	nodes defined as	s P-1, 2, 3 et	c. Pipe are re	ferenced			
	on supplied map	o entitled "Pipe Name	es."						
<u>Start Node</u> :	Node where pip	e section starts.							
End Node:	Node where pip	e section ends.							
Node Elevation	on: Elevation of not	le above sea level. El	evations are det	ermined by	converting				
	Easting/Northing	g coordinates from su	pplied customer	map throug	h CoordTrans	s to assign			
	elevations to eac	h node.							
Node Pressur	e: Pressure of node	given in pounds per	square inch.						
Pressure Hea	d: The height of a	column of fluid of spe	cific weight. T	his is what t	he pump mus	t overcome			
	to function.								
Length:	Distance of pipe	between two junction	n nodes.						
Diameter:	Nominal pipe di	ameters are given in t	he report. The l	below table s	shows the act	ual pipe			
	diameter for the	different types of pip	e.						
	Nominal Pipe Dia.	SDR 21 / SDR 26	SCHED 40	DR-9	DR-11				
	1.25	1.556	1.38	1.27	1.34				
	1.5	1.754	1.61	1.453	1.533				
	2	2.193	2.067	1.815	1.917				
	2.5	2.655	2.489		·				
	3	3.43	3.068	2.675	2.826				

3	3.43	3.068	2.675	2.826
4	4.154	4.026	3.44	3.633
5	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		4.253	4.49
6	6.115	6.08	5.065	5.349
8	7.961	7.981	6.594	6.963
10	9.924	10.02	8.219	8.679
12	11.77	11.938	9.746	10.293

<u>Flowrate</u>: <u>Velocity</u>: Amount of water in gallons per minute flowing through the pipeline. Given in feet per sec. This is how fast the water is traveling through the pipeline.

Attached Maps:

All attached maps are formatted to 34"x 44." While these maps can be printed on standard $8\frac{1}{2}$ x 11, we recommend the larger print form for visual clarity. These maps can be printed by request if necessary equipment is not available to produce plots of this size.

The results contained in this hydraulic analysis were developed utilizing information given to Pentair Pump Group Inc.("we" or "us") by representatives of the community or other parties involved in the planning and design of the system. This information was then input into KYPIPE 2000, an independent software program not owned or designed by us. We are not responsible for the accuracy of the provided information or the operation of the software. Accordingly, we cannot guarantee these same results will be experienced upon installation of pumps.

Formula to Determine Number of Pumps to Run Simultaneously at Peak Flow (Based on Ohio EPA Design Standards)

Peak Factor x Average Daily Flow = **Peak Hourly Design Flow** (GPD)

Peak factor is calculated using the following equation.

 $\frac{3.33 \ x \ 24 \ hours}{Run - off \ period \ (hours)} = Peak \ Factor$

(this peak factor used unless specified otherwise by engineer)

The average daily flow is calculated using the following equation.

Number of Units x Gallons per Day per Unit = Average Daily Flow (GPD)

The Peak Hourly Design Flow can then be calculated and is then converted to GPM by the following equation.

 $\frac{Peak Hourly Design Flow (GPD)}{24 Hours/_{Day} \times 60 Minutes/_{Hour}} = Daily GPM$

By dividing the Daily GPM by the average flow of the pumps selected for the system, the number of pumps running at one time can be determined.

 $\frac{Daily GPM}{Average GPM of Pump} = Total Number of Pumps to Run Simultaneously$

The number of pumps calculated above, are placed in the system in the worst case locations. These locations would include areas with the greatest elevation change and the ends of the force main. Additional pumps may be placed in system to verify operation of pumps in multiple areas.

Peak Factor = 3.33 Daily Flow per Lot = 12254 Avg. GPD Pump Chosen to Simulate: Myers VS50 & VS30 (Avg. GPM = 75)

Average Daily Flow

3 EDU's x 12254 Avg. GPD = 36762 GPD

Peak Hourly Design Flow

3.33 x 36762 GPD = 122417.46 GPD

Daily Flow

 $\frac{122417.46 GPD}{24 Hours/Day \times 60 Minutes/Hour} = 85.01 GPM$

Number of Pumps to Run Simultaneously

 $\frac{85.01 \text{ GPM}}{75 \text{ GPM}} = Approximately 2 \text{ pump}(s) \text{ to run simulatenously at peak flow}$

Pipe Material Chosen: SDR-21

C-Factor: 120

A percentage of total pumps shown on model. 2 pump(s) picked to run in model.

Node Analysis

Node Name	Node Elevation (ft)	Pressure Head (ft)	Node Pressure (psi)	
J-5	211.6	38.7	16.8	
J-7	212.3	41.5	18.0	
R-1	225.5	0.0	0.0	
O-VB-1	214.6	214.6 41.4		
O-VB-2	210.1	43.7	19.0	
O-VB-3	O-VB-3 206.5 45.2		19.6	
O-Pump-1	200.1	67.3	29.2	
O-Pump-2	213.9	42.1	18.3	
O-Pump-3	204.4	49.4	21.4	
I-VB-1	214.6	41.4	17.9	
I-VB-2	210.1	43.7	19.0	
I-VB-3	206.5	45.2	19.6	

Node Analysis Complete



Pipeline Analysis

Pipe Name	Start Node	End Node	Length (ft)	Diameter (in)	FlowRate (gpm)	Velocity (ft/s)	Head Loss (ft)
P-1	O-Pump-3	I-VB-2	571.7	3.2	0.0	0.0	0.0
P-2	O-Pump-2	J-5	172.7	3.2	109.0	4.5	5.7
P-3	J-5	R-1	676.3	4.1	224.1	5.6	24.8
P-4	O-Pump-1	I-VB-1	1070.4	4.1	115.1	2.9	11.4
P-5	J-7	I-VB-3	201.9	4.1	115.1	2.9	2.2
P-6	O-VB-1	J-7	201.5	4.1	115.1	2.9	2.2
P-7	O-VB-2	J-7	325.6	3.2	0.0	0.0	0.0
P-8	O-VB-3	J-5	125.7	4.1	115.1	2.9	1.3

Pipe Type: SDR-21 C-Factor: 120

Pipeline Analysis Complete



Pump Analysis

Pump Name	Pump Type	Flowrate (gpm)	Pump Elevation (ft)	Pump Head (ft)	Pump Pressure (psi)	Notes
Pump-1	VS50	115.1	200.1	67.3	29.2	
Pump-2	VS30	109.0	213.9	42.1	18.3	
Pump-3	VS30	0.0	204.4	49.4	21.4	Pump off

Pump Analysis Complete



Item Inventory

Pipes

Ріре Туре	Pipe Diamter (in)	Number	Total Length (ft)	Notes		
SDR-21	3	3	1070			
SDR-21	4	5	2276			
	Total	8	3346			
Pumps						

VS50	3	5HP - 3 Phase pumps (1 Triplex)
VS30	4	3HP - 1 Phase Pumps (2 Duplex)

Notes



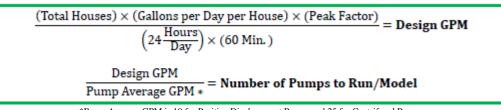
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C-Factor: 120

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O-VB-3	O-VB-3 206.5 39.0		16.9
O-Pump-1	200.1	64.6	28.0
O-Pump-2	213.9	28.5	12.3
O-Pump-3	204.4	57.1	24.8
I-VB-1	214.6	38.2	16.5
I-VB-2	210.1	44.4	19.3
I-VB-3	206.5	39.0	16.9

Node Analysis Complete



Pipeline Analysis

Pipe Name	Start Node	End Node	Length (ft)	Diameter (in)	FlowRate (gpm)	Velocity (ft/s)	Head Loss (ft)
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P-5	J-7	I-VB-3	201.9	4.1	181.8	4.5	5.0
P-6	O-VB-1	J-7	201.5	4.1	117.7	2.9	2.3
P-7	O-VB-2	J-7	325.6	3.2	64.1	2.6	4.0
P-8	O-VB-3	J-5	125.7	4.1	181.8	4.5	3.1

Pipe Type: SDR-21 C-Factor: 120

Pipeline Analysis Complete



Pump Analysis

Pump Name	Pump Type	Flowrate (gpm)	Pump Elevation (ft)	Pump Head (ft)	Pump Pressure (psi)	Notes
Pump-1	VS50	117.7	200.1	64.6	28.0	
Pump-2	VS30	0.0	213.9	28.5	12.3	Pump off
Pump-3	VS30	64.1	204.4	57.1	24.8	

Pump Analysis Complete



Item Inventory

Pipes

Pipe Type	Pipe Diamter (in)	Number	Total Length (ft)	Notes			
		1					
SDR-21	3	3	1070				
SDR-21	4	5	2276				
<u>.</u>		-					
Total		8	3346				
Pumps							
Pump Type	Number	Notes					
VS50	3	5HP - 3 Phase pumps (1 Triplex)					

3HP - 1 Phase Pumps (2 Duplex)



VS30

4